RE: Report of
Geotechncial Engineering Investigation
INDOT Project No. STP-9969
DES No. 0100667 Road Replacement
East Pearl Street from Park Avenue to
Coonhunter Road (Co. Rd. 300E)
Batesville, Indiana
Ripley County
Seymour District
Patriot Project No. 1-03-0557

# Prepared For:

Mr. Ben Carnahan Bonar Group 6420 Castleway West Drive Indianapolis, IN 46250

# Prepared By:

Patriot Engineering and Environmental, Inc. 600 North Weinbach Av. Suite 920 Evansville, Indiana 47711

October 10, 2003



Mr. Ben Carnahan Bonar Group 6420 Castleway West Drive Indianapolis, IN 46250

RE: Report of

> Geotechnical Engineering Investigation INDOT Project No. STP-9969 () DES. No. 0100667Road Replacement East Pearl Street - from Park Avenue to Coonhunter Road Batesville, Indiana

Ripley County Seymour District

Patriot Project No. 1-03-0557

#### Dear Ben:

Attached is the report of our subsurface investigation for the above referenced project. This report includes detailed boring logs of fourteen (14) test borings drilled on East Pearl Street from Station 11+00 to Station 53+00 in Batesville, Indiana, plus four (4) additional test borings on Line B for a proposed storm sewer. Also included in the report are the results of laboratory tests performed on samples obtained from the site, and geotechnical recommendations pertinent to the site development and construction.

We appreciate the opportunity to have performed this geotechnical engineering investigation and are looking forward to working with you during the construction phase of the project. If you have any questions regarding this report or if we may be of any additional assistance regarding any geotechnical aspect of the project, please do not hesitate to contact our office

Respectfully submitted.

Patriot Engineering and Environmental, Inc.

Richard L. Johnson, P.E.

Senior Project Engineer

60018167

Consulting Environmental, Geotechnical and Materials Engineers Offices in Indianapolis, Evansville, Ft. Wayne, Lafayette, Terre Haute and Louisville, KY

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# SUMMARY OF RECOMMENDATIONS Geotechnical Investigation Des No.: 0100667 Project No.: STP-9969 ()

Road Replacement -East Pearl Street Ripley County, Batesville, Indiana Seymour District

Patriot Project No. 1-03-0557

## Roadway and Pavement

In general, medium stiff to very stiff fine-grained soils were encountered in the roadway borings. Over most of the alignment the upper three feet of soil is also medium stiff to stiff. The natural moisture content of the fine-grained soils in the upper three feet of soil ranged from 17 to 22 percent, averaging 18 percent at the road boring locations. These moisture contents are approximately 3 to 8 percent above optimum, averaging about 4 percent over optimum. Medium dense sandy loam fill was noted in the upper three feet in three of the borings with moisture contents of 15 to 22 percent.

The grade of the majority of the project will not be significantly changed. The Average Annual Daily Traffic (AADT) for East Pearl Street is greater than 2,000 vehicles per day (vpd) for year 2000 and is projected to 6,620 vpd by 2020. Because the total subgrade area is greater than 10,000 square yards, **Type A** Subgrade Treatment is recommended. A CBR value of 3 could be used for pavement design.

We recommend longitudinal subsurface drains due to the low permeability of the on-site soil. The subsurface drains should be constructed in accordance with the procedures outlined in Section 718, "Underdrains", of the State Specifications. Since the subgrade soil is primarily clay loam, a geotextile filter fabric shall be utilized in accordance with INDOT Standard Specifications (ISS) 718.04.

## Structures

The subgrade conditions at the invert elevations of the storm sewers evaluated during this investigation are suitable for placement of the structures. Some local undercutting of soft soils may be necessary. Proposed invert elevations extend up to 3 feet below the limestone bedrock at 2 locations for the storm sewer along East Pearl Street and up to 5 feet below the limestone bedrock or auger refusal depth for the Line B Storm Sewer. In addition, groundwater may be encountered during construction near the invert elevation. Temporary dewatering methods are recommended herein for these structures.

\*This summary is a brief synopsis of our geotechnical recommendations. This summary is not intended to be used for design or construction purposes. We recommend that the designer and contractors read the entire geotechnical engineering investigation report for complete recommendations.

# REPORT OF GEOTECHNICAL ENGINEERING INVESTIGATION

Geotechnical Investigation Des No.: 0100667 Project No.: STP-9969 () Road Replacement - East Pearl Street from North Park Avenue to Coonhunter Road Ripley County, Batesville, Indiana Seymour District

Patriot Project No. 1-03-0557

## 1.0 INTRODUCTION

#### 1.1 General

The proposed project involves the replacement of a segment of East Pearl Street from North Park Avenue easterly to Coonhunter Road (Co. Rd. 300E) in Batesville, Indiana. The new roadway will be 24 feet wide (two 12-foot wide lanes), and a new storm sewer will be constructed.

The results of the geotechnical engineering investigation for this project are presented in this report. This investigation was carried out in general accordance with INDOT's standard procedures.

#### 1.2 Purpose and Scope

The purpose of this investigation is to determine the general near surface and subsurface conditions within the project area and to develop the geotechnical engineering recommendations necessary for design and construction of the storm sewers and roadway replacement. This was achieved by drilling test borings at sixteen (16) locations plus two additional hand auger holes for a proposed retaining wall on the south side of East Pearl Street. This report contains the results of our findings, an engineering interpretation of these results with respect to the available project characteristics, and recommendations to aid in the design and construction of the storm sewers and road replacement.

## 2.0 PROJECT INFORMATION

The proposed project includes the replacement of a segment of East Pearl Street located in Batesville, Indiana. The western terminus is the intersection of East Pearl Street and Park Avenue (Station 10 + 95). The eastern terminus is at the intersection of Coonhunter Road (Station 53 + 00). The project length is approximately 4,205 lineal

feet, (0.80 miles). We understand a new sewer is proposed along most of the project's length (from about Station 11 + 07 to 51 + 70 except for a 199 foot long segment between Station 37 + 09 to 39 + 10). A Vicinity and Boring Location Map are presented in Appendix A.

# 3.0 INVESTIGATIONAL PROCEDURES

## 3.1 Field Work

A total of eighteen (18) test borings were performed at the project site at the approximate locations as shown on the Boring Location Map (in Appendix A).

On June 25 to June 27, 2003, Roadway Borings RB-1 through RB- 8 were drilled on East Pearl Street to a depth of 10 to 20.5 feet below the existing ground surface in accordance with INDOT Exhibit "C" (Requirements For Geotechnical Investigation and Pavement Investigation) Section D-4-B. The borings were advanced using 31/4-inch I.D. hollow-stem augers. Samples were recovered in the undisturbed material below the bottom of the augers using the standard drive sample technique (SPT) in accordance with (AASHTO T206). A 2-inch O.D. by 13/8 inch I.D. split-spoon sampler was driven a total of 18 inches with the number of blows of a 140-pound hammer falling 30 inches recorded for each 6 inches of penetration. The sum of blows for the final 12 inches of penetration is the Standard Penetration Test result commonly referred to as the N-value (or blow-count). The splitspoon samples were typically recovered at 2.5 feet intervals, beginning at a depth of 1 foot below the existing surface grades, extending until boring termination. A rock core sample was obtained from the auger refusal depth of 10.5 feet in RB-3 to the termination depth of 20.5 feet. The core sample was obtained using a standard double tube NX core barrel with a diamond cutting bit. Water levels were monitored at each borehole location during drilling and upon completion.

Four (4) additional Roadway Borings (RB-13 through RB-16) were obtained from side roads near the intersection with East Pearl Street. Borings RB-14 through RB-16 were extended to a depth of 10 feet using the same soil drilling procedures detailed in the previous paragraph. Boring RB-13 on Line S-3-A was extended to auger refusal at 18.1 feet, and a rock core sample was taken from 18.5 to 28.5 feet.

Four (4) additional borings (RB-9 through RB-12) were taken for the Line B storm sewer that will be constructed from Eastern Avenue to Tekulve Avenue. These borings were extended from 8.4 feet to 19 feet. Rock core samples were taken from 9.0 to 19.0 feet in

RB-10 and from 10.8 to 19.0 feet in RB-11. Again, the same soil drilling and coring procedures were used for these borings.

Two borings were also attempted using hand auger equipment for the proposed retaining wall (RB-17 and RB-18). These borings met refusal at depths of 10 and 8 inches, respectively, and the borings were terminated at those depths without any sampling.

Upon completion of the boring program, all of the samples retrieved in this sampling program were returned to *Patriot's* soil testing laboratory where they were visually examined and placed in groups of like material. A laboratory-generated log of each boring has been prepared based upon the driller's field log, laboratory test results, and visual classification. Test boring logs and a field classification system for soil exploration is included, in Appendix A, in this report. Indicated on each log is the primary strata encountered, the depth of each stratum change, the depth of sample, Standard Penetration Test results, groundwater conditions, and selected laboratory test data. The laboratory logs were prepared for each boring giving the appropriate sample data and the textural description and classification.

# 3.2 Laboratory Testing

Representative samples recovered in the borings were selected for testing in the laboratory to evaluate their physical properties and engineering characteristics. Laboratory analysis included: natural moisture content determinations (AASHTO T265); Grain Size Analysis (AASHTO T88); Atterberg Limits (AASHTO T89 and T90), Unconfined Compressive Strength (AASHTO T208), Standard Proctor Test (AASHTO T99), California Bearing Ratio Test (AASHTO T193), Soil pH, and an estimate of the unconfined compressive strength (Qu) of the cohesive soil samples utilizing a calibrated hand penetrometer. Subgrade Resilient Modulus Testing (AASHTO T 307-99) was performed on the same sample that was used for the California Bearing Ratio test. The Resilient Modulus Tests was performed by Boudreau Engineering in Suwanee, Georgia. The results of all laboratory tests are summarized in Appendix B. Soil descriptions on the boring logs are in general accordance with the AASHTO system and the INDOT Standard Specifications (ISS¹) (textural classification, e.g., clay loam).

## 4.0 SITE AND SUBSURFACE CONDITIONS

#### 4.1 Site Conditions

The project site is located Batesville, Indiana. *Patriot* visited the site on June 19, 2003, prior to drilling, to stake boring locations and to make visual observations regarding the site.

The project site is currently a two-lane road surrounded by industrial facilities and commercial businesses. Bonar Group provided a site plan and profile. The existing road is generally level.

#### 4.2 Subsurface Conditions

Our interpretation of the subsurface conditions is based upon eighteen (18) widely spaced test borings, drilled at the approximate locations shown on the Boring Location Map in Appendix A. The following discussion is general; for more specific information, please refer to the boring logs presented in Appendix A. It should be noted that the dashed stratification lines shown on the soil boring logs indicate approximate transitions between soil types. In situ stratification changes could occur gradually or at different depths. All depths discussed below refer to depths below the existing ground surface.

All sixteen (16) of the truck borings were drilled through existing pavement. Beneath the asphalt pavement in Borings RB-1 through RB-8 where the asphalt ranged from 5 to 10 inches with an average thickness of about 6.5 inches, a layer of crushed stone was encountered ranging in thickness from 9 to 17 inches with an average of 12.25 inches. Total (asphalt plus crushed stone) pavement thickness ranged from 15 to 23 inches and averaged about 19 inches.

Over the length of the project, generally five major soil types were encountered beneath the surface material. The soil is comprised of Clay, Clay Loam, two different Loam groups, and Silty Clay Loam.

The **clay loam** (Test #2, Summary Sheet, Appendix A) was found directly below the crushed stone base course in RB-3 through 5, RB-7 and RB-8 and RB-14. It was also found beneath a layer of sandy loam/loam fill in RB-1, RB-9 and RB-16, beneath a layer of silty clay loam in RB-6 and RB-15 and beneath a layer of clay in RB-7. The thickness of the clay loam ranged from 1.5 to 12 feet and averaged 5.5 feet over the length of the

project. The consistency of the clay loam ranged from very soft to very stiff with SPT N-values ranging from 3 to 25 blows per foot (bpf) as based on INDOT blow count criteria.

The **silty clay loam** (Test #4, Summary Sheet, Appendix A), was encountered in RB-1 from 13.5 to 15 feet, in RB-2 from 3.5 to 5.0 feet, in RB-6 from below the pavement to 3.5 feet and in RB-15 from 3.5 to 6.0 feet. The thickness of the silty clay loam ranged from 1.5 to 2.5 feet. The consistency of the silty clay loam ranged from very soft to very stiff with SPT N-values ranging from 2 to 25 blows per foot (bpf) as based on INDOT blow count criteria.

The **clay** (Test #1, Summary Sheet, Appendix A) was found directly below the clay loam (Test #2) in RB-1, RB-2, RB-4 through 7 and RB-16 and below the silty clay loam (Test #4) in RB-2. The thickness of the clay ranged from 2.5 to 8.5 feet and averaged 4.7 feet over the length of the project. The consistency of the clay ranged from medium stiff to stiff with SPT N-values ranging from 7 to 12 blows per foot (bpf) as based on INDOT blow count criteria.

The **loam** (Test #3, Summary Sheet, Appendix A), where present (RB-2, 3, 7, 8, and 13) was found either below the clay loam (Test #2), below silty clay loam (Test #4) or below crushed stone fill generally below a depth of 13.5 feet and extending to limestone bedrock. An exception was noted in RB-3, where the loam layer was found from 8.5 to 13.5 feet. The thickness of the loam ranged from 1 to 5 feet and averaged 3.6 feet over the length of the project. The consistency of the loam was generally very stiff to very hard with SPT N-values ranging from 46 to more than 80 blows per foot (bpf) as based on INDOT blow count criteria. The exception was in RB-13, where the very soft loam layer was located beneath a crushed stone fill layer and an N-value of 2 bpf was noted.

The **loam** (Test #5, Summary Sheet, Appendix A), where present (RB-2), was a fill layer found below the pavement at a depth of 1.5 to 3.5 feet. The consistency of the loam was medium stiff with an SPT N-value of 7 blows per foot (bpf) as based on INDOT blow count criteria.

It should be noted that a layer of sandy loam fill was noted beneath the pavement in RB-1, 15 and 16. This sandy loam fill layer was found to be about 2 feet thick and was medium dense with SPT N-values of 11 to 28 bpf.

#### 4.3 Groundwater Conditions

Groundwater was encountered during drilling in 4 Borings (RB-2, RB-3, RB-7 and RB-13) at depths of 9.2 to 14.5 feet below the existing ground surface. After the borings were completed and the augers were removed from the boreholes, water was measured in RB-2 at 15.8 feet while RB-7 was dry. The water level at completion of drilling RB-3 and RB-13 was obscured by water introduced into the borehole for rock coring. A 24-hour water reading of 7.0 feet was obtained from RB-2.

It should be recognized that fluctuations in the groundwater level should be expected to occur due to variations in rainfall and other environmental or physical factors at the time measurements are made. The true static groundwater level can only be determined through observations made in cased holes over a long period of time, the construction of which was beyond the scope of this investigation.

# 5.0 DESIGN RECOMMENDATIONS

#### 5.1 Basis

Our recommendations are based on data presented in this report, which include soil borings, laboratory testing and our experience with similar projects. Subsurface variations, that may not be indicated by a dispersive exploratory boring program, can exist on any site. If such variations or unexpected conditions are encountered during construction, or if the project information is incorrect or changed, we should be informed immediately since the validity of our recommendations may be affected. Refer to Appendix C for additional qualifications and contractual considerations.

# 5.2 Subgrade Considerations

In general, medium stiff to stiff soil was encountered in the roadway borings. Over most of the alignment the upper three feet of soil is also medium stiff to stiff. The natural moisture of the upper three feet of soil ranged from 17 to 22 percent and averaged 18 percent at the road boring locations. One Proctor test was performed on representative of the clay loam soil from the upper three feet. The optimum moisture for the clay loam (CBR 1 from Station 21+50) was 14.0 percent at a maximum dry density of 110 pcf. Therefore, the existing natural moisture of the upper three feet of soil is approximately 4% above

optimum, ranging from 3 to 8 percent over optimum.

Exceptions to these general soil subgrade conditions were noted in several of the roadway borings on Line PR-1 and on the side roads. Medium dense sandy loam or loam fill was found beneath the pavement in RB-1, RB-2, RB-15 and RB-16 extending to a depth of 3.5 feet at each location. This fill was black to gray in color and contained crushed stone and asphalt. STP N-values in the sandy loam were 11 to 28 bpf, and moisture contents were 15 to 21 percent. An STP N-value of 7 bpf and a moisture content of 32 percent were found in the loam layer in RB-2. Crushed stone fill was found beneath the pavement to a depth of 13.5 feet in RB-13. N-values ranged from 11 bpf down to 2 bpf in this layer.

## Cut and At-Grade Sections

The grade of the majority of the project will not be significantly changed. The Average Annual Daily Traffic (AADT) for East Pearl Street is greater than 3,000 vehicles per day (vpd), through 2020. Because the total subgrade area is greater than 10,000 square yards, **Type A** Subgrade Treatment is recommended. Type A treatment for fine-grained subgrade soils involves the following options: (1) chemical soil modification of the upper 16 inches, or (2) over-excavating 12 inches and replacement with No. 53 coarse aggregate. (An alternate treatment is suggested in Appendix C to reduce the amount of over-excavation.)

A California Bearing Ratio test and Resilient Modulus tests were also performed on sample CBR-1 from RB-3. This sample represents the predominant soil type for the project. The California Bearing Ratio test yielded a CBR value of 2.9 percent at 97 percent compaction. The Resilient Modulus test yielded a M<sub>R</sub> values ranging from 7,600 to 12,700, based on 15 cycles of testing at various combinations of Chamber Confining Pressure and Maximum Axial Stress applied to samples compacted to about 95 percent at optimum moisture content and at 2 percent over optimum.

Assuming proper subgrade preparation (see below and Section 6.0), a CBR value of 3 values is based on a sample compacted at +2 percent and a 2 psi Confining and Axial pressures.) We further recommend that the subgrade be prepared in accordance with Section 207, "Subgrade", of the INDOT Standard Specifications.

## **Other Considerations**

Pockets of soft or wet soil may be encountered especially if poor weather conditions prevail during construction. Undercuts, if required, should be performed in general accordance with Section 203 of the INDOT Standard Specifications. Prior to placement of new fill, all existing surfaces should be stripped of vegetation and benched in accordance with Section 203 of the ISS.

If grading is performed in very favorable weather conditions, undercutting or drying may not be required. However, wet weather conditions will have deleterious effects on the clay loam, silty clay loam and clay subgrade. During wet periods, it is anticipated that the surficial soils will not pass proofrolling and would have to be dried and recompacted, or it may be necessary to undercut prior to the placement of new fill or pavement section. Care should be taken during construction not to disturb or wet the subgrade soils. All deleterious materials and unsuitable soil encountered during roadway excavations should be removed and replaced with recompacted suitable soil.

# 5.3 Longitudinal Pavement Subsurface Drains

As discussed, the near surface subgrade soils are clayey and loamy in nature with relatively high moisture conditions (3 to 8 percent over optimum). Therefore, we recommend installing longitudinal subsurface drains throughout the length of the project in conjunction with transverse subsurface drains as necessary in locally depressed areas along the pavement profile. The subsurface drains should be constructed in accordance with the procedures outlined in Section 718, "Underdrains", of the State Specifications. Since the subgrade soil is primarily clay loam and silty clay loam soil, a geotextile filter fabric shall be utilized in accordance with INDOT Standard Specifications (ISS) 718.04. Construction of subsurface drains may be difficult in these urban conditions, due to buried utilities and obstructions that could slow construction and increase the project cost. Consideration should be given to eliminating some subsurface drains, depending upon subsoil conditions, in areas where shallow buried utilities could be a significant problem.

# 5.4 Drainage Structures

Road borings were extended to depths ranging from 10 to 20.5 feet to provide data for the 12 to 48-inch diameter storm sewer and appurtenant manhole structures that extend through the entire length of the project. The soil near the proposed invert elevation is suitable for supporting these structures. However, it should be noted that the proposed invert elevations at RB-3 and RB-13 (Line S-3-A) are below the depth at

which bedrock was encountered. Therefore, the proposed invert elevation may be about 3 feet below the limestone bedrock surface at those locations.

Four (4) other borings were extended to depths of 8.4 to 19 feet to provide data for the 60-inch diameter to 5 feet by 3 feet to 29.5 square feet deformed pipe to 6 feet by 3 feet storm sewer (Line B) and appurtenant manhole structures that will extend from Eastern Avenue to Tekulve Avenue. The soil near the proposed invert elevation is suitable for supporting these structures. However, it should be noted that the proposed invert elevation at RB-9 through RB-11 (Line B) is below the depth at which bedrock was encountered in RB-10 and RB-11 and below the auger refusal depth (and estimated bedrock surface in RB-9). Therefore, the proposed invert elevation may be about 3 to 5 feet below the limestone bedrock surface near RB-9, about 2 to 4 feet below the limestone surface at RB-10 and about 1 foot below the rock surface at RB-11.

In addition, pH testing of 5 representative samples indicated pH values between 7.3 and 7.6, with an average of about 7.45, indicative of generally neutral soils.

Note that pockets of soft, wet or otherwise unsuitable materials may be encountered at the bearing grade and may require undercutting to achieve the above bearing capacities. Proper subgrade inspection during construction will be critical to keep settlements within tolerable limits. In addition, several of the borings indicate that water is close to or just below the invert elevation for some of the structures (see borings RB-2, 3, 7 and 13.) Temporary dewatering during construction should be expected in these areas. Dewatering recommendations are presented in Section 6.4 below.

# 5.5 Retaining Wall

Two low modular block retaining walls are proposed for this project. One wall extends from about Station 19+25 to 24+25 and the second from about Station 49+25 to 50+35. Both walls will be located about 20 to 22 feet right of Line "PR-1", and both will be a maximum of 3 to 3.5 feet in height. Two hand auger borings (RB-17 and RB-18) were attempted to investigate the subsurface conditions for these walls. Neither boring could be advanced beyond a depth of 10 inches. Boring RB-3 was drilled at Station 21+50, 2 feet right of "PR-1", and RB-8 was drilled at Station 50+98, 3 feet right of "PR-1". Stiff to very stiff clay loam soil was encountered from 2.5 to 4 feet below the pavement surface in RB-3 and from 2 to 3.5 feet in RB-8. Based on the resistance encountered by the hand auger borings and the stiff to very stiff clay loam soils in RB-3 and RB-8, the foundation soils are suitable for the support of these low walls for a maximum toe pressure of 2,000

pounds per square foot (psf), provided that the recommendations included in Section 6.3 of this report are followed.

## 6.0 CONSTRUCTION CONSIDERATIONS

## 6.1 Site Preparation

Site preparation should be performed in general compliance with Section 201 "Clearing and Grubbing" of the latest edition of the Indiana Department of Transportation (INDOT) Standard Specifications. Prior to placement of embankment fill, foundations, structure backfill, or base course materials, all topsoil and other unsuitable materials must be removed from within the embankment/pavement section. Unsuitable materials include; frozen soil, relatively soft material, old fill, relatively wet soils, deleterious material, or soils near the surface that exhibit a high organic content. Deeper undercutting may be required in localized areas such as at existing ditch lines, buried drain tiles, and culverts.

## 6.2 Roadway Excavation and Embankment Construction

The removal of existing structures and obstructions within the construction limits shall be performed in general compliance with Section 202 "Removal of Structures and Obstructions" of the Specifications. Backfilling of open excavations at these structures should be performed in accordance with Section 203.23 "Embankment Over and Around Structures" of the Specifications.

As a general practice, we recommend proofrolling of all exposed surfaces within the limits of proposed embankment construction to delineate local soft or disturbed areas. As indicated in Section 5.2, the near surface had in-situ moisture contents above the optimum moisture content. These soils may become soft during grading and require additional treatment depending on the conditions encountered during construction. General construction requirements for preparation and construction of embankment areas should be performed in compliance with all applicable parts of "Excavation and Embankment – General Construction Requirements", Section 203.09 of the Specifications.

#### 6.3 Shallow Foundation Excavations

Upon completion of the foundation excavations and prior to the placement of reinforcing steel, the exposed subgrade should be checked to confirm that a bearing surface of adequate strength has been reached. Any localized soft soil zones encountered at the bearing elevations should be further excavated until adequate support soils are

encountered. The cavity should be backfilled with structural fill as defined below, or the footing can be poured at the excavated depth. Structural fill used as backfill beneath footings should be limited to lean concrete, well-graded sand and gravel, or crushed stone placed and compacted in accordance with Section 6.2.

If it is necessary to support spread footings on structural fill, the fill pad must extend laterally a minimum distance beyond the edge of the footing. The minimum structural pad width would correspond with a point at which an imaginary line extending downward from the outside edge of the footing at a 1H:2V slope intersects the surface of the natural soils. For example, if the depth to the bottom of excavation is 4 feet below the bottom of the foundation, the excavation would need to extend laterally beyond the edge of the footing at least 2 feet.

Excavation slopes should be maintained within OSHA requirements. In addition, we recommend that any surcharge fill or heavy equipment be kept at least 5 feet away from the edge of the excavation.

#### 6.4 Groundwater

Groundwater was encountered during drilling in 4 borings at depths of 9.2 to 14.5 feet below the existing ground surface. After the borings were completed and the augers were removed from the boreholes, water was measured at 1 boring location (RB-2) at a depth of 15.8 feet below the existing ground surface. A 24-hour water reading was obtained from boring RB-2 at a depth of 7 feet.

Groundwater inflow into shallow excavations above the water table is expected to be adequately controlled by conventional methods such as gravity drainage and/or pumping from sumps. More significant inflow can be expected in deeper excavations below the groundwater table requiring more aggressive dewatering techniques, such as well or wellpoint systems.

# 7.0 LIMITATIONS OF INVESTIGATION

The recommendations provided herein were developed from the information obtained in the test borings, which depict subsurface conditions only at specific locations. Subsurface conditions at other locations may differ from those occurring at the specific drill sites.

The nature and extent of variations between borings may not become evident until the course of construction. If variations become evident, it will be necessary to re-evaluate the recommendations of this report after performing on-site observations during the excavation and noting the characteristics of any variation.

Our professional services have been performed, findings obtained, and recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices. This warranty is in lieu of all other warranties either expressed or implied. This company is not responsible for the independent conclusions, opinions or recommendations made by others based on the field and laboratory data presented in this report.

The scope of our services did not include any environmental assessment or investigation for the presence or absence of wetlands, hazardous or toxic materials in the soil, groundwater, or surface water within or beyond the site studied. Any statements in this report or on the test borings logs regarding vegetation types, odors or staining of soils, or other unusual conditions observed are strictly for the information of our client and the owner.

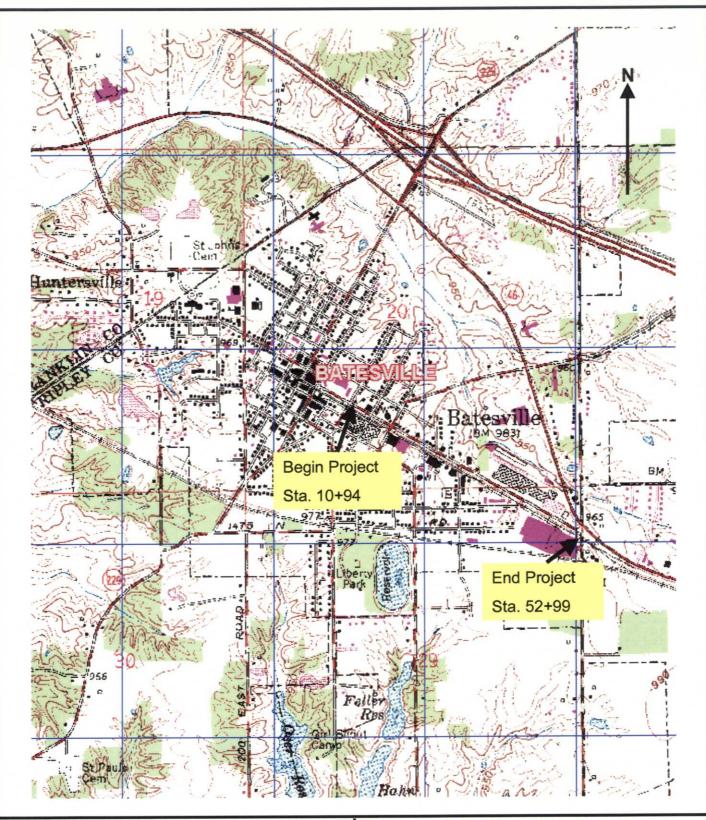
# APPENDIX A

VICINITY MAP (Figure 1)

BORING LOCATION MAP (Figure 2)

**BORING LOG KEY** 

**BORING LOGS** 





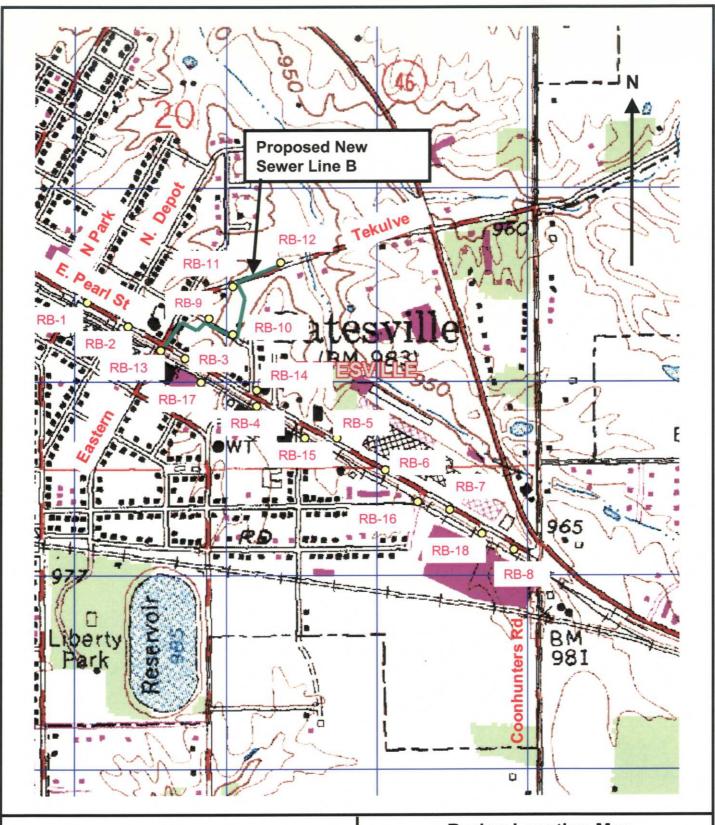
# **Site Vicinity Map**

East Pearl St. Rehabilitation Batesville, Indiana STP 9969 (), Des No. 0100667

Job No.

1-03-0557

Figure





# PATRIOT ENGINEERING

and Environmental, Inc. Indianapolis, IN 46250

# **Boring Location Map**

East Pearl St. Rehabilitation Batesville, Indiana STP- 9969 ( ), Des No. 0100667

Job No.

1-03-0557

Figure

## **BORING LOG KEY**

# AASHTO FIELD CLASSIFICATION SYSTEM FOR SOIL EXPLORATION

#### NON COHESIVE SOILS

(Silt, Sand, Gravel and Combinations)

| L                   | Density                                  |               | Grain Size Terminolo | ogy                    |
|---------------------|--|---------------|----------------------|------------------------|
| Very Loose<br>Loose | 5 blows/ft, or less<br>6 to 10 blows/ft. | Soil Fraction | Particle Size        | US Standard Sieve Size |
| Medium Dense        | 11 to 30 blows/ft.                       | Boulders      | Larger than 75mm     | Larger than 75mm       |
| Dense               | 31 to 50 blows/ft.                       | Gravel:       | 2.00mm to 75mm       | #10 to 75mm            |
| Very Dense          | 51 blows/ft. or more                     | Sand: Coarse  | 0.42mm to 2.00mm     | #40 to #10             |
| ***                 |  | Fine          | 0.075mm to 0.42mm    | #200 to #40            |
|                     |  | Silt          | 0.002mm to 0.075mm   | Smaller than #200      |
|                     |  | Clay          | Smaller than 0.002mm | Smaller than #200      |

#### RELATIVE PROPORTIONS FOR SOILS

| Descriptive Term | Percent |
|------------------|---------|
| Trace            | 1 - 10  |
| Little           | 11 - 20 |
| Some             | 21 - 35 |
| And              | 36 - 50 |

#### **COHESIVE SOILS**

(Clay, Silt and Combinations)

| C            | onsistency           | Field Identification                       | Unconfined Compressive<br>Strength (tons/sq. ft.) |
|--------------|----------------------|--|---|
| Very soft    | 3 blows/ft. or less  | Thumb will penetrate soil more than 1 inch | Less than 0.25                                    |
| Soft         | 4 to 5 blows/ft.     | Thumb will penetrate soil about 1 inch     | 0.25 - 0.5  |
| Medium Stiff | 6 to 10 blows/ft.    | Thumb will penetrate soil about ½ inch     | 0.5 - 1.0   |
| Stiff        | 11 to 15 blows/ft.   | Thumb will indent soil about 1/4 inch      | 1.0 - 2.0   |
| Very Stiff   | 16 to 30 blows/ft.   | Readily indented by thumbnail              | 2.0 - 4.0   |
| Hard         | 31 blows/ft. or more | Indented with difficulty by thumbnail      | Over 4.0  |

Classification on logs are made by visual inspection.

<u>Standard Penetration Test</u> - Driving a  $2.0^{\circ}$  O.D.,  $1^{3/8}$  I.D., sampler a distance of 1.0 foot into undisturbed soil with a 140 pound hammer free falling a distance of 30.0 inches. It is customary for **Patriot** to drive the spoon 6.0 inches to seat into undisturbed soil, then perform the test. The number of hammer blows for seating the spoon and making the tests are recorded for each 6.0 inches of penetration on the drill log (Example - 6/8/9). The standard penetration test results can be obtained by adding the last two figures (i.e. 8 + 9 = 17 blows/ft.).

<u>Strata Changes</u> - In the column "Soil Descriptions" on the drill log the horizontal lines represent strata changes. A solid line (----) represents an actually observed change, a dashed line (----) represents an estimated change.

<u>Groundwater</u> observations were made at the times indicated. Porosity of soil strata, weather conditions, site topography, etc., may cause changes in the water levels indicated on the logs.

Groundwater symbols: ▼-observed groundwater elevation, encountered during drilling; ∇-observed groundwater elevation upon completion of boring.



#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Bonar Group Client:

Boring No.: RB-1

Page 1 of 1

Surface Elevation: 972.5 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 () Structure No.: N/A

0100667

Station: 11+50 Weather: Sunny

Offset: Temp:

10 feet Rt

Line: A

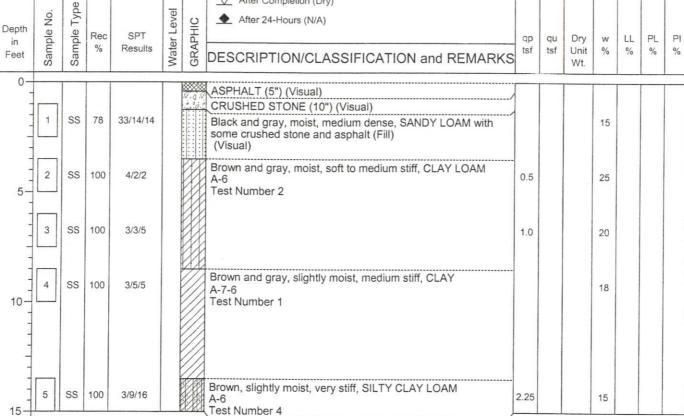
Des. No.: Cave-In Depth: 9.5 feet Start Date: 6/25/03

90 0 End Date: 6/25/03

Driller: R. Sumler Mobile B-61

Remarks:

| T     |   | Water Level             |    |
|-------|---|-------------------------|----|
|       |   | ■ During Drilling (Dry) |    |
|       |   |                         |    |
| Level | 2 | ◆ After 24-Hours (N/A)  |    |
| _     | 0 |                         | qp |



Boring terminated at 15 feet.

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#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-2

Page 1 of 1

Surface Elevation: 970.0 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 ()

Structure No.: N/A Des. No.: 0100667 Station:

15+50 Weather: Sunny

Start Date: 6/25/03

Offset: Temp:

6 feet Rt 90 0

End Date: 6/25/03

Line:

Driller: R. Sumler

Rig: Mobile B-61

Cave-In Depth: 16 feet Remarks: Water Level ▼ During Drilling (14.5 feet) Sample Type Water Level Sample No. After 24-Hours (7 feet) GRAPHIC Depth Rec SPT in qu Dry qp LL PL % Results tsf Feet tsf Unit % % % % DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0. ASPHALT (5") (Visual) CRUSHED STONE (12") (Visual) 1 SS 60 9/4/3 Dark gray and black, moist, medium stiff, LOAM with trace 0.5 32 crushed stone and asphalt (Fill) Brown, moist, very soft, SILTY CLAY LOAM 2 SS 70 2/1/1 A-6 0.25 30 5 Test Number 4 Brown and gray, moist, stiff, CLAY 3 ST 58 1.8 111.3 18 A-7-6 (44) Test Number 1 SS 4 85 3/5/6 2.0 25 66 20 46 10 Brown, slightly moist, very stiff, LOAM with trace SS 40 23/25/29 5 weathered limestone 14 15 Test Number 3  $\nabla$ 6 SS 20 50-6" Brown, wet, weathered, LIMESTONE fragments (Visual) 20 Boring terminated at 19 feet.

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0100667

Des. No.:

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#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Bonar Group Client:

Boring No.: RB-3

Page 1 of 1

Surface Elevation: 963.7 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 () Station: 21+50 Structure No.: N/A Weather: Sunny

Offset: 2 feet Rt Temp: 90 0 End Date: 6/25/03

Line: PR-1 Driller: R. Sumler Rig: Mobile B-61

Cave-In Depth: 10 feet Remarks:

Start Date: 6/25/03

| Depth      | e No.      | Sample Type | Rec | SPT     | Level       | HIC     | Water Level  ✓ During Drilling (9.2 feet)  ✓ After Completion (Obscured due to rock coring.)  ◆ After 24-Hours (N/A)  |           |           | -                  |        |         | 5       | 1       |
|------------|------------|-------------|-----|---------|-------------|---------|---|-----------|-----------|--------------------|--------|---------|---------|---------|
| in<br>Feet | Sample No. | Sampl       | %   | Results | Water Level | GRAPHIC | DESCRIPTION/CLASSIFICATION and REMARKS  | qp<br>tsf | qu<br>tsf | Dry<br>Unit<br>Wt. | w<br>% | LL<br>% | PL<br>% | PI<br>% |
| 0-         |            | SS          | 75  | 4/6/7   |             | 0.00    | ASPHALT (5") (Visual)  CRUSHED STONE (17") (Visual)  Gray to brown, slighty moist, stiff, CLAY LOAM A-6 (16) Test Number 2                                  | 2.0       |           |                    | 22     | 40      | 14      | 26      |
| -          | 2          | SS          | 60  | 5/5/6   |             |         |   | 2.0       |           |                    | 14     |         |         |         |
| 10-        | 3          | SS          | 95  | 8/13/33 |             |         | Brown, slightly moist, hard, LOAM with wet sand seam at 9.2 feet A-6 (4) Test Number 3 Auger refusal at 10.5 feet Rockcore from 10.5 to 20.5 feet. RQD= 33% | 4.5+      |           |                    | 9      | 26      | 12      | 14      |
| 15-        | 4          | RC          | 86  |         |             |         | Lt gray, slightly weathered fine to medium grained LIMESTONE with fossils and a weathered shale seam from 17 to 17.3 feet (Visual)                          |           |           |                    |        |         |         |         |

Boring terminated at 20.5 feet.



#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-4

Page 1 of 1

Surface Elevation: 967.3 feet Patriot Project No.: 1-03-0557

STP 9969 () Project No.: Structure No.: N/A

Station: Weather: Sunny

Remarks:

27+50

Offset: 3 feet Rt Temp:

90 0

Line: PR-1

Des. No.: 0100667 Cave-In Depth: 5 feet Start Date: 6/25/03 End Date: 6/25/03 Driller: R. Sumler Rig: Mobile B-61

Water Level ▼ During Drilling (Dry) Sample Type Water Level Sample No. After 24-Hours (Dry) GRAPHIC Depth Rec SPT Dry qp qu in % Results tsf tsf % Unit Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0-ASPHALT (6") (Visual) CRUSHED STONE (17") (Visual) Brown and gray, slightly moist, medium stiff, CLAY LOAM 10/4/4 SS 60 1 18 Test Number 2 2 SS 4/4/5 0.75 16 Gray and brown, moist, medium stiff, CLAY 3 SS 100 3/4/6 1.0 22 A-7-6 Test Number 1 4 SS 80 3/3/4 1.0 26

Boring terminated at 10 feet.

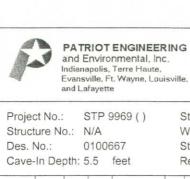
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Sample Type

Rec

%

Sample No.

1 SS 70

2 SS 80

3 SS 100

4

10

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20-

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SS 75

Depth

in

Feet

0

Water Level

SPT

Results

4/8/6

4/5/7

4/5/6

4/5/6

GRAPHIC

#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-5

Page 1 of 1

Surface Elevation: 969.2 feet Patriot Project No.: 1-03-0557

Station: 33+50 Offset: 10 feet Lt Line: PR-1 Weather: Sunny 90 0 Temp: Driller: R. Sumler Start Date: 6/25/03 End Date: 6/25/03 Rig: Mobile B-61 Remarks: Water Level ▼ During Drilling (Dry) ☑ After Completion (Dry) After 24-Hours (Dry) qp qu Dry PL LL tsf % tsf Unit % % DESCRIPTION/CLASSIFICATION and REMARKS Wt. ASPHALT (7") (Visual) CRUSHED STONE (12") (Visual) Brown and gray, slightly moist, stiff, CLAY LOAM with crushed stone layer at 3 feet (Fill) 1.75 17 A-6 Test Number 2 Brown and gray, slightly moist, stiff, CLAY LOAM 1.5 16 Test Number 2 Gray and brown, moist, stiff, CLAY 1.25 24 A-7-6 Test Number 1 1.0 20

Boring terminated at 10 feet.



#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-6

Page 1 of 1

Surface Elevation: 970.0 feet Patriot Project No.: 1-03-0557

STP 9969 () Project No.: Structure No.: N/A

Station:

39+50 Weather: Cloudy Offset:

6 feet Lt 85 °

Line: PR-1 Driller: R. Sumler

Temp:

Rig:

Mobile B-61

Des. No.: 0100667 Start Date: 6/26/03 End Date: 6/26/03 Cave-In Depth: 6.8 feet Remarks: Water Level ▼ During Drilling (Dry) ☑ After Completion (Dry) Sample Type Water Level ◆ After 24-Hours (N/A) GRAPHIC Depth Sample Rec SPT Dry PL qp qu LL in % Results tsf tsf Unit % Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0-ASPHALT (10") (Visual) CRUSHED STONE (9") (Visual) Gray and brown, sligthly moist, stiff, SILTY CLAY LOAM A-6 (20) SS 40 9/7/6 1.25 17 40 16 24 Test Number 4 Brown and gray, Slighty moist, stiff, CLAY LOAM 2 SS 85 4/6/6 2.0 13 A-6 Test Number 2 Gray, slightly moist to moist, medium stiff CLAY 3 SS 20 4/5/5 1.0 19 A-7-6 Test Number 1 4 SS 100 3/4/6 1.0 24 10

Boring terminated at 10 feet.

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LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group Boring No.: RB-7

Page 1 of 1

Surface Elevation: 970.2 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 () Station: 46+13 Offset: 3 feet Rt Line: PR-1 85 ° Structure No.: N/A Weather: Cloudy Temp: Driller: R. Sumler Des. No.: 0100667 Start Date: 6/26/03 End Date: 6/26/03 Rig: Mobile B-61 Cave-In Depth: 10.5 feet Remarks: Water Level During Drilling (13.5 feet) ☑ After Completion (Dry) Sample Type Water Level Sample No. After 24-Hours (N/A) GRAPHIC Depth Rec SPT Dry PL qp qu LL in % Results Unit Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0. ASPHALT (7") (Visual) CRUSHED STONE (11") (Visual) Gray and brown, slightly moist, stiff to medium stiff, CLAY 1 SS 60 5/6/6 2.0 17 LOAM A-6 Test Number 2 2 5/4/5 1.0 SS 90 18 Fuel odor observed at 2 feet. Gray and brown, slightly moist, stiff, CLAY 3 SS 100 3/5/7 1.75 18 A-7-6 Test Number 1 Brown, moist, stiff, CLAY LOAM 4 SS 100 5/6/6 1.5 21 A-6 Test Number 2 10-5 SS 75 8/17/35 4.5 Brown, slightly moist, hard, LOAM A-6 15 Test Number 3 Boring terminated at 15 feet. 20 08-04-2003 I:\Mtech2002\Projects\2003\1-0557\RB-7.bor 25



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#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group Boring No.: RB-8

Page 1 of 1

Surface Elevation: 970.1 feet Patriot Project No.: 1-03-0557

STP 9969 () Project No.: Station: 50+98 Offset: 3 feet Rt Line: PR-1 Structure No.: N/A Weather: Cloudy 85 ° Temp: Driller: R. Sumler Des. No.: 0100667 Start Date: 6/26/03 End Date: 6/26/03 Rig: Mobile B-61 Cave-In Depth: 8 feet Remarks: PR-1 Water Level ▼ During Drilling (Dry) Sample Type Water Level Sample No. After 24-Hours (N/A) GRAPHIC Depth Rec SPT Dry ap qu LL PL in % Results tsf Unit % % Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt 0. ASPHALT (8") (Visual) CRUSHED STONE (10") (Visual) Gray and brown, slightly moist, stiff to very stiff, CLAY LOAM SS 3/4/7 1 85 2.0 19 A-6 Test Number 2 2 SS 20 5/5/6 2.0 15 3 SS 100 5/7/11 2.75 17 4 SS 100 6/11/14 3.25 18 10 Brown, slightly moist, hard, LOAM SS 80 15/29/50-4" 4.5+ 9 Test Number 3 15 (Gray, weathered, LIMESTONE (Visual) 20 Boring terminated at 18.7 feet. 25



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#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group Boring No.: RB-9

Page 1 of 1

Surface Elevation: 954.2 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 () Station: 13+73 Offset: 4 feet Rt Line: Structure No.: N/A Weather: Sunny 78° Temp: Driller: R. Sumler Des. No.: 0100667 Start Date: 6/27/03 End Date: 6/27/03 Rig: Mobile B-61 Cave-In Depth: 6 Remarks: Water Level ▼ During Drilling (Dry) Sample Type Water Level Sample No. ◆ After 24-Hours (N/A) GRAPHIC Depth Rec SPT qp qu Dry PL in LL % Results tsf tsf % Unit % Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0 ASPHALT (5") (Visual) CRUSHED STONE (7") (Visual) Dark gray to brown, moist, soft, LOAM with trace brick (Fill) SS 3/2/2 1 50 23 Test Number 5 Brown, slightly moist, medium stiff, CLAY LOAM 2 SS 80 2/3/3 1.0 18 Test Number 2 5 3 SS 90 4/9/21 4.0 19 Brown, slightly moist, very stiff, LOAM A-6 Test Number 3 50-5" Auger refusal at 8 feet. Gray, weathered, LIMESTONE (Visual) 10 Boring terminated at 8.4 feet. 15 20 25 30



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#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group Boring No.: RB-10

Page 1 of 1

Surface Elevation: 951.4 feet Patriot Project No.: 1-03-0557

Project No .: STP 9969() Station: 15+74 Offset: 3 feet Lt Line: B Structure No.: N/A Weather: Sunny Temp: 78 ° Driller: R. Sumler Des. No.: 0100667 Start Date: 6/27/03 End Date: 6/27/03 Rig: Mobile B-61 Cave-In Depth: 8 feet Remarks: Water Level During Drilling (6.5 feet) Type Level After 24-Hours (N/A) GRAPHIC Depth Sample . Rec SPT Water PL gp qu Dry W LL in % Results tsf Unit % % Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0 ASPHALT (3") (Visual) (CRUSHED STONE (7") (Visual) Dark gray and brown, moist, soft, CLAY LOAM with trace 1 SS 70 4/2/2 0.25 26 brick (Fill) Test Number 2 2 SS 75 3/2/1 0.25 25 3 3/4/4 SS 85 Wet sand seam at 6.4 feet 1.0 21 Brown and gray, moist, medium stiff to hard, CLAY A-7-6 4 SS 5 50-2" 19 Test Number 1 Auger Refusal at 9 feet Lt gray, weathered, fine to medium grained LIMESTONE 10 Dark gray, slightly weathered, fine to medium grained, LIMESTONE interbedded with weathered shale seams (Visual) 5 RC Dark Gray with It gray partings, slightly weathered fine to medium grained, LIMESTONE (Visual) 15 20 Boring terminated at 19 feet. 25



PATRIOT ENGINEERING and Environmental, Inc. Indianapolis, Terre Haute, Evansville, Ft. Wayne, Louisville, and Lafayette LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-11

Page 1 of 1

Surface Elevation: 947.6 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 ()

Structure No.: N/A Des. No.: 0100667 Station:

20+04 Weather: Cloudy Offset: 10 feet Lt

85 ° Temp:

Line: B

Driller: R. Sumler

Cave-In Depth: 8 feet

Start Date: 6/26/03 Remarks:

End Date: 6/27/03

Rig: Mobile B-61

|            |            | be          |          |                | _           |         | Water Level  During Drilling (Dry)  After Completion (Obscured due to rock coring.) |           |     |             |    |    |    |   |
|------------|------------|-------------|----------|----------------|-------------|---------|---|-----------|-----|-------------|----|----|----|---|
| epth<br>in | Sample No. | Sample Type | Rec<br>% | SPT<br>Results | Water Level | GRAPHIC | ◆ After 19-Hours (7.3 feet)   | qp<br>tof | qu  | Dry         | W  | LL | PL | F |
| eet        | San        | San         | %        | Results        | Wat         | GR/     | DESCRIPTION/CLASSIFICATION and REMARKS  | tsf       | tsf | Unit<br>Wt. | %  | %  | %  |   |
| 0-         |            |             |          |                |             |         | ASPHALT (10") (Visual)  |           |     |             |    |    |    | Γ |
| =          |            |             |          |                |             |         | CRUSHED STONE (6") (Visual)   |           |     |             |    |    |    |   |
| -          | 1          | SS          | 80       | 2/2/3          |             |         | Brown, slightly moist, soft to medium stiff, CLAY LOAM A-6                          | 0.5       |     |             | 19 |    |    |   |
| -          | Ш          |             |          |                |             |         | Test Number 2   |           |     |             |    |    |    |   |
| 7          | 2          | SS          | 20       | 4/4/5          |             |         |   | 0.75      |     |             | 18 |    |    |   |
| 5-         |            |             |          |                |             |         |   | 0.70      |     |             | 10 |    |    |   |
| -          |            |             |          |                |             |         |   |           |     |             |    |    |    |   |
| 1          | 3          | SS          | 90       | 5/8/9          |             |         | Brown, slightly moist, very stiff, LOAM<br>A-6                                      | 4.0       |     |             | 11 |    |    |   |
| -          |            |             |          |                |             |         | Test Number 3   |           |     |             |    |    |    |   |
| -          |            |             |          |                |             |         |   |           |     |             |    |    |    |   |
| 0-         | 4          | SS          | 100      | 5/8/13         |             |         |   | 4.0       |     |             | 14 |    |    |   |
| F          | _          |             |          |                |             |         | Auger refusal at 10.8 feet, flush with pavement, begin rockcoring on 6/27/03.       |           |     |             |    |    |    |   |
| =          |            |             |          |                |             |         | Rock core from 10.8 to 19.0 feet, RQD= 9%   |           |     |             |    |    |    |   |
| 1          |            |             |          |                |             |         | Lt gray, weathered , fine to medium grained LIMESTONE                               |           |     |             |    |    |    |   |
| =          |            |             |          |                |             |         | \interbedded with shale and clay seams (Visual)                                     |           |     |             |    |    |    |   |
| -          |            |             |          |                |             |         | Dark gray weathered SHALE interbedded with limestone (Visual)                       |           |     |             |    |    |    |   |
| 5          | 5          | RC          | 50       |                |             |         |   |           |     |             |    |    |    |   |
| -          |            |             |          |                |             |         | Note: Rockcoring terminated at 19 feet due to poor water circulation                |           |     |             |    |    |    |   |
| -          |            |             |          |                | 1           |         |   |           |     |             |    |    |    |   |
| -          |            |             |          |                | 100         |         |   |           |     |             |    |    |    |   |
| İ          |            |             |          |                | t           |         |   |           |     |             |    |    |    | _ |

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#### LOG OF TEST BORING

East Pearl Street Road Rehabilitation

Client:

Location: Batesville, Indiana Bonar Group

Boring No.: RB-12

Page 1 of 1

Surface Elevation: 965.0 feet Patriot Project No.: 1-03-0557

Project No.:

STP 9969 () Structure No.: N/A

Station: Weather: Sunny

25+29

Offset: Temp:

10 feet Rt

78°

Line: B

Driller: R. Sumler

Des. No.:

0100667

Start Date: 6/27/03

End Date: 6/27/03

Rig: Mobile B-61

Cave-In Depth: 11 Remarks: feet Water Level ▼ During Drilling (Dry) Water Level After 24-Hours (N/A) GRAPHIC Sample 1 Depth Rec SPT Dry in % Results tsf Unit % % % % DESCRIPTION/CLASSIFICATION and REMARKS Feet Wt. 0 ASPHALT (8") (Visual) CRUSHED STONE (6") (Visual) Gray and brown, slightly moist, medium stiff, LOAM (Fill) 1.0 15 1 SS 80 4/5/4 A-6 (4) Test Number 5 12 28 13 Gray and brown, moist, medium stiff to stiff, CLAY LOAM 19 2 SS 90 3/3/5 Test Number 2 1.0 20 3 SS 100 3/4/6 SS 100 2.0 19 4 4/6/6 10 Gray and brown, moist, very stiff, CLAY 7/7/9 2.25 24 5 SS 95 A-7-6 Test Number 1 15 Boring terminated at 15 feet.

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LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Bonar Group Client:

Boring No.: RB-13

Page 1 of 1

Surface Elevation: 969.2 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 () Structure No.: N/A

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0100667

Station: Weather:

9+55 Sunny

Offset: 10 feet Rt Temp: 90 0

Line: S-3-A Driller: R. Sumler

End Date: 6/25/03

Rig: Mobile B-61

Des. No.: Start Date: 6/25/03 Cave-In Depth: 7 Remarks: feet Water Level ▼ During Drilling (13 feet) Sample Type Water Level Sample No. After 24-Hours (N/A) GRAPHIC Depth Rec SPT Dry PL qp qu % Results tsf tsf Unit Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. ASPHALT (6") (Visual) CRUSHED STONE (Visual) (Fill) 1 SS 80 8/6/5 2 SS 5/4/4 60 3 SS 20 2/2/2 4 SS 2/1/1 20 10 Brown, wet, very soft, LOAM 5 SS 40 1/1/1 33 A-6 Test Number 3 15 • Auger refusal at 18.1 feet SS 50-3" <u>\_6</u> 10 Rockcore from 18.5 to 28.5 feet, RQD= 48 % Lt gray, slightly weathered, fine to medium grained LIMESTONE (Visual) 20 08-01-2003 I:\Mtech2002\Projects\2003\1-0557\RB-13.bor RC 80 25 Dark gray weathered SHALE (Visual) Lt gray, slightly weathered, fine to medium grained LIMESTONE interbedded with shale seams (Visual)

Boring terminated at 28.5 feet.



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LOG OF TEST BORING
Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-14

Page 1 of 1

Surface Elevation: 969.0 feet Patriot Project No.: 1-03-0557

| Project<br>Structor<br>Des. N<br>Cave- | ure No.:   | 0.: 0       | N/A<br>01006 |                | Weather: Sunny Temp: 90 ° Di Start Date: 6/25/03 End Date: 6/25/03 Remarks: |         |  |           |           |                    |        | Line: S-4-A Driller: R. Sumler Rig: Mobile B-61 |         |     |  |  |  |  |  |
|--|------------|-------------|--------------|----------------|---|---------|--|-----------|-----------|--------------------|--------|---|---------|-----|--|--|--|--|--|
| Depth<br>in<br>Feet                    | Sample No. | Sample Type | Rec<br>%     | SPT<br>Results | Water Level   | GRAPHIC | Water Level  ✓ During Drilling (Dry)  ✓ After Completion (Dry)  ◆ After 24-Hours (N/A)  DESCRIPTION/CLASSIFICATION and REMARKS | qp<br>tsf | qu<br>tsf | Dry<br>Unit<br>Wt. | w<br>% | LL<br>%   | PL<br>% | P % |  |  |  |  |  |
| 0-                                     |            |             |              |                |   | 0.00    | ASPHALT (3") (Visual)  |           |           |                    |        |   |         |     |  |  |  |  |  |
| -                                      | 1          | SS          | 100          | 3/4/6          |   |         | CRUSHED STONE (5") (Visual)  Brown and gray, sightly moist, medium stiff to stiff, CLAY LOAM A-6                               | 1.0       |           |                    | 16     |   |         |     |  |  |  |  |  |
| 5-                                     | 2          | SS          | 80           | 5/4/4          |   |         | Test Number 2  | 1.0       |           |                    | 18     |   |         |     |  |  |  |  |  |
| 1                                      | 3          | SS          | 100          | 3/4/6          |   |         |  | 1.0       |           |                    | 19     |   |         |     |  |  |  |  |  |
| 10                                     | 4          | SS          | 70           | 4/5/6          |   |         |  | 1.0       |           |                    | 17     |   |         |     |  |  |  |  |  |
| -                                      |            |             |              |                |   |         | Boring terminated at 10 feet.  |           |           |                    |        |   |         |     |  |  |  |  |  |
| 15-                                    |            |             |              |                |   |         |  |           |           |                    |        |   |         |     |  |  |  |  |  |
| -                                      |            |             |              |                |   |         |  |           |           |                    |        |   |         |     |  |  |  |  |  |
| 20-                                    |            |             |              |                |   |         |  |           |           |                    |        |   |         |     |  |  |  |  |  |
|  |            |             |              |                |   |         |  |           |           |                    |        |   |         |     |  |  |  |  |  |
| -                                      |            |             |              |                |   |         |  |           |           |                    |        |   |         |     |  |  |  |  |  |



Depth

in

#### PATRIOT ENGINEERING and Environmental, Inc. Indianapolis, Terre Haute,

Evansville, Ft. Wayne, Louisville, and Lafayette

LOG OF TEST BORING

East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-15

Page 1 of 1

Surface Elevation: 970.4 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 ()

Structure No.: N/A Des. No.: 0100667

Station: Weather:

9+50 Sunny Offset:

10 feet Rt

Temp: 90 ° End Date: 6/25/03 Line: S-6-A

Driller: R. Sumler Rig: Mobile B-61

Cave-In Depth: 6.7 feet

Rec

%

SPT

Results

Remarks:

Start Date: 6/25/03

Water Level

▼ During Drilling (Dry)

☑ After Completion (Dry)

After 24-Hours (N/A)

DESCRIPTION/CLASSIFICATION and REMARKS

qp tsf tsf

qu

Dry LL Unit % %

%

Water Level Sample No. GRAPHIC Sample % Feet Wt. 0 ASPHALT (6") (Visual) CRUSHED STONE (12") (Visual) Black, slightly moist, medium dense, SANDY LOAM with crushed stone and asphalt (Fill) SS 80 6/7/7 16 (Visual) Gray and brown, slightly moist, medium stiff, SILTY CLAY SS 2 70 4/3/3 0.75 LOÁM 13 A-6 Test Number 4 Gray and brown, moist, medium stiff, CLAY LOAM 3 SS 100 3/3/5 1.0 23 A-6 Test Number 2 Fuel odor observed at 6feet SS 100 3/4/6 4 0.75 22 10

Boring terminated at 10 feet.

10-10-2003 I:\Mtech2002\Projects\2003\1-0557\RB-15.bor

15

20-

25

30



PATRIOT ENGINEERING and Environmental, Inc. Indianapolis, Terre Haute, Evansville, Ft. Wayne, Louisville, and Lafayette

#### LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-16

Page 1 of 1

Surface Elevation: 971.5 feet Patriot Project No.: 1-03-0557

Project No.: STP 9969 ()

Structure No.: N/A

Station: Weather: Cloudy

9+60

Offset: Temp:

13 feet Rt 85 °

Line: S-7-A Driller: R. Sumler

Des. No.:

0100667

Start Date: 6/26/03

End Date: 6/26/03

Mobile B-61

Cave-In Depth: 7 Remarks: Water Level ▼ During Drilling (Dry) ☑ After Completion (Dry) Sample Type Level After 24-Hours (N/A) GRAPHIC Depth Rec SPT Dry Water I in Results % tsf tsf Unit % % % % Feet DESCRIPTION/CLASSIFICATION and REMARKS Wt. 0 ASPHALT (11") (Visual) CRUSHED STONE (10") (Visual) Black and gray, moist, medium dense, SANDY LOAM with 4/5/6 SS 90 crushed stone and asphalt (Fill) 21 A-2 (Visual) Gray and Brown, moist, very soft, CLAY LOAM 2 SS 80 2/1/2 0.25 18 A-6 5 Test Number 2 Gray and brown, slightly moist, medium stiff, CLAY 1.6 110.3 18 3 ST 56 Test Number 1 SS 100 3/3/5 1.0 20 10

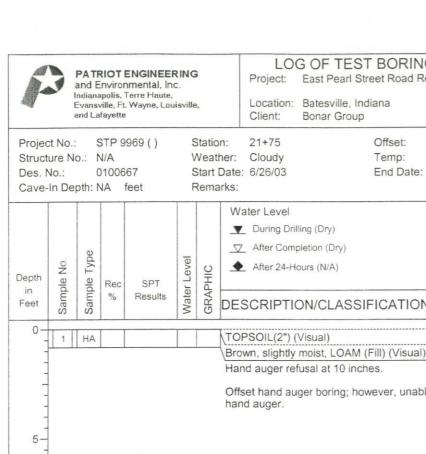
Boring terminated at 10 feet.

15

20-

25

30



10

15

20

25

30

08-04-2003 I:\Mtech2002\Projects\2003\1-0557\RB-17.bor

## LOG OF TEST BORING

Project: East Pearl Street Road Rehabilitation

Location: Batesville, Indiana Client: Bonar Group

Boring No.: RB-17

Page 1 of 1

Surface Elevation: 967.50 feet Patriot Project No.: 1-03-0557

21+75 Offset: 21 feet Rt Line: "PR-1" 85 ° Weather: Cloudy Temp: Driller: R. Sumler Start Date: 6/26/03 End Date: 6/26/03 Rig: Mobile B-61 Water Level ▼ During Drilling (Dry) ☑ After Completion (Dry) After 24-Hours (N/A)

Dry PL LL qu qp tsf Unit % % % DESCRIPTION/CLASSIFICATION and REMARKS Wt.

Hand auger refusal at 10 inches. Offset hand auger boring; however, unable to advance the hand auger.

## **APPENDIX B**

Summary of Classification Test Data

Particle Size Distribution Reports

**Unconfined Compressive Strength Test Curves (Qu)** 

**Standard Proctor Test Curve** 

**CBR Test Curve** 

Summary of CBR Test Data

**Resilient Modulus Test Data** 

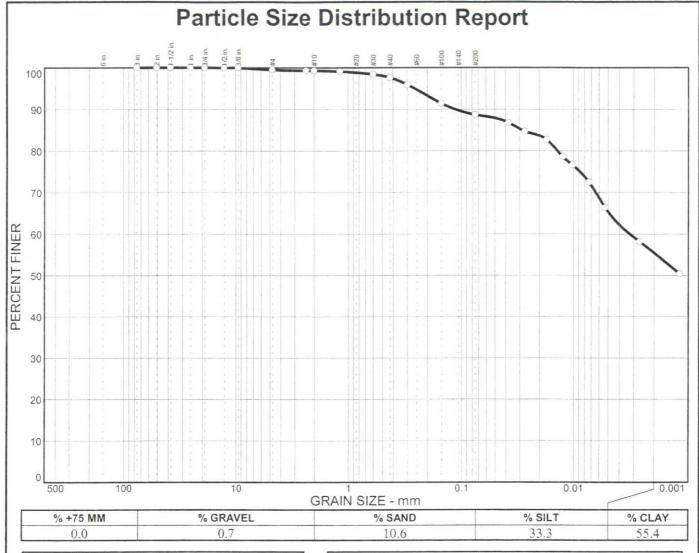


PATRIOT ENGINEERING and Environmental, Inc. 6330 East 75th Street, Suite 216 Indianapolis, IV 46250-2700 (317) 576-8058 FAX. (317) 576-1965

SUMMARY OF CLASSIFICATION TESTS DATA

| INDOT Project Number: STP-9969 (), DES# 0100667 | tipley District: Seymour | Sonar Group Client Address: 6420 Castleway West Drive, Indianapolis, IN 46250 |
|---|--------------------------|---|
| abilitation, Batesvill                          | County:                  | Client:   |
| East Pearl Street Road Reh                      | N/A                      | 1-03-0557   |
| Project Name:                                   | Structure No.:           | Patriot Proj. No.:  |

|         | _  |   |   |  |  |  |
|---------|--|---|---|--|--|--|
|         | Ы  | 46  | 26  | 14   | 24   | 15   |
|         | Ы  | 20  | 14  | 12   | 16   | 13   |
|         | 1  | 99  | 40  | 26   | 40   | 28   |
|         | Hd                                       | 7.3   | 7.6   | 7.5  | 7.4  | 7.5  |
| %       | Clay                                     | 55.4  | 29.0  | 15.0   | 25.8   | 16.4   |
| %       | Silt                                     | 33.3  | 42.1  | 37.5   | 8.09   | 36.6   |
| %       | Sand                                     | 10.6  | 24.8  | 39.1   | 11.0   | 31.8   |
| %       | Gravel                                   | 0.7   | 4.1   | 8.4  | 2.4  | 15.2   |
|         | #200                                     | 88.7  | 71.1  | 52.5   | 9.98   | 53.0   |
|         | #40                                      | 97.6  | 89.2  | 81.0   | 94.7   | 78.7   |
|         | _  |   | 95.9  | 91.6   | 97.6   | 84.8   |
|         | AASHTO                                   | A-7-6(44)   | A-6(16)   | A-6(4)   | A-6(20)  | A-6(4)   |
|         | Textural                                 | CLAY  | CLAY LOAM   | LOAM   | SILTY CLAY LOAM  | LOAM   |
| Depth   | ft.                                      | 8.5-10  | 2-6   | 8.5-10   | 2-3.5  | 1.5-3  |
| Sample  | Number                                   | S-4   | CBR-1   | S-3  | S-1  | S-1  |
| Offset  |  | 6 ft. Rt. "A"   | 2 ft. Rt. "PR-1"  | 2 ft. Rt. "PR-1"   | 6 ft. Lt. "PR-1"   | 25+29 10 ft. Rt. "B"   |
| Station |  | 15+50   | 21+50   | 21+50  | 39+50  | 25+29  |
| Boring  | Number                                   | RB-2  | RB-3  | RB-3   | RB-6   | RB-12  |
| Test    | nper                                     | _   | 2   | 3  | 4  | 5  |
|         | Boring Station Offset Sample Depth % % % | Boring         Station         Offset         Sample         Depth         AASHTO         #10         #40         #200         Gravel         Sand         Silt         Clay         PH         LL         PL | Station         Offset         Sample         Depth         AASHTO         #10         #40         #200         Gravel         88.7         90.3         97.6         88.7         10.6         33.3         55.4         7.3         66         20 | Station         Offset         Sample         Depth         AASHTO         #10         #40         #200         Gravel         % | Station         Offset         Sample         Depth         AASHTO         #10         #40         #200         Gravel         % | Station         Offset         Sample         Depth         AASHTO         #10         #40         #200         Gravel         % |



| SIEVE   | PERCENT   | SPEC.*  | PASS?  |
|---|---|---------|--------|
| SIZE  | FINER   | PERCENT | (X=NO) |
| 3 in.<br>2 in.<br>1 -1/2 in.<br>1 in.<br>3/4 in.<br>1/2 in.<br>3/8 in.<br>#4<br>#8<br>#10<br>#16<br>#30<br>#40<br>#50<br>#100<br>#200 | 100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>99.5<br>99.3<br>99.3<br>99.1<br>98.4<br>97.6<br>95.9<br>91.4<br>88.7 |         |        |

|   | Soil Description                         |  |
|---|--|--|
| Brown and gray  | V, CLAY, $pH = 7.3$                      |  |
|   |  |  |
| PL= 20  | Atterberg Limits                         | PI= 46                                 |
| 1 L- 20   |  | 1 1- 40                                |
| D <sub>85</sub> = 0.0285  | Coefficients<br>D <sub>60</sub> = 0.0033 | D <sub>50</sub> =                      |
| D <sub>85</sub> = 0.0285<br>D <sub>30</sub> =<br>C <sub>u</sub> = | D <sub>15</sub> =                        | D <sub>50</sub> =<br>D <sub>10</sub> = |
| o <sub>u</sub> -  | OC                                       |  |
| USCS=   | Classification<br>AASHT                  | TO= A-7-6(44)                          |
|   | Remarks                                  |  |
|   |  |  |
|   |  |  |

Sample No.: S-4

Source of Sample:

Date: 7-18-03

Location: Stat: 15+50, 6 ft. Rt. "A"

Elev./Depth: 8.5'-10'

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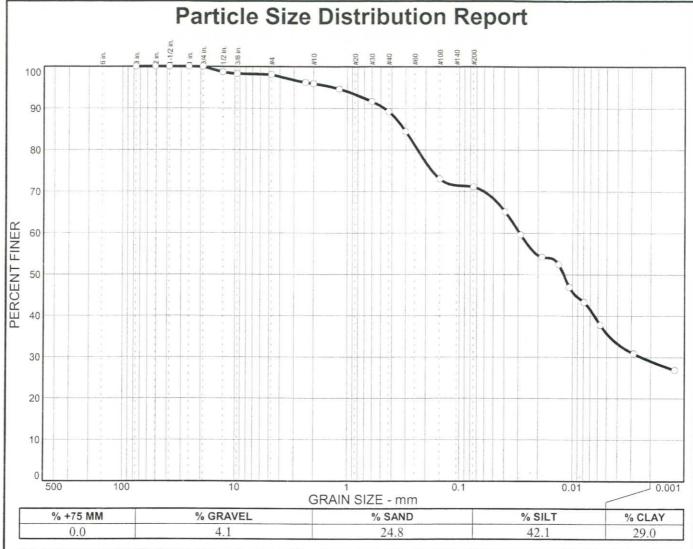
and Environmental, Inc.

Client: Bonar Group

Project: East Pearl Street Road Rehabilitation, Batesville, Indiana

STP 9969(), DES# 0100667

Project No: 1-03-0557



| SIEVE  | PERCENT   | SPEC.*  | PASS?  |
|--|---|---------|--------|
| SIZE   | FINER   | PERCENT | (X=NO) |
| 3 in.<br>2 in.<br>1-1/2 in.<br>1 in.<br>3/4 in.<br>1/2 in.<br>3/8 in.<br>#4<br>#10<br>#16<br>#30<br>#40<br>#50<br>#100 | 100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>98.7<br>98.3<br>98.1<br>96.2<br>95.9<br>94.6<br>91.6<br>89.2<br>84.4<br>73.0<br>71.1 |         |        |

|   | Soil Description  | 1   |
|---|---|---|
| Brown, CLAY   | LOAM, $pH = 7.6$  |   |
|   |   |   |
| PL= 14  | Atterberg Limits  | PI= 26  |
| D <sub>85</sub> = 0.311<br>D <sub>30</sub> = 0.0024<br>C <sub>u</sub> = | Coefficients<br>D <sub>60</sub> = 0.0292<br>D <sub>15</sub> =<br>C <sub>c</sub> = | D <sub>50</sub> = 0.0120<br>D <sub>10</sub> = |
| USCS=   | Classification<br>AASH1   | TO= A-6(16)                                   |
|   | Remarks   |   |
|   |   |   |
|   |   |   |

Sample No.: CBR-1

Source of Sample: RI

RR-3

Date: 7-18-03

Location: Stat: 21+50, 2 ft. Rt. "PR-1"

Elev./Depth: 2-6 ft.

PATRIOT ENGINEERING

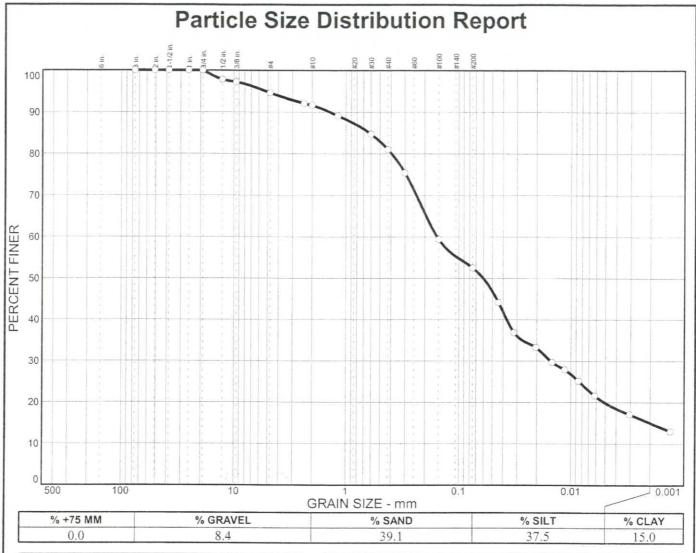
Client: Bonar Group

Project: East Pearl Street Road Rehabilitation, Batesville, Indiana

STP 9969(), DES# 0100667

and Environmental, Inc.

Project No: 1-03-0557



| SIEVE  | PERCENT   | SPEC.*  | PASS?  |
|--|---|---------|--------|
| SIZE   | FINER   | PERCENT | (X=NO) |
| 3 in.<br>2 in.<br>1 -1/2 in.<br>1 in.<br>3/4 in.<br>1/2 in.<br>3/8 in.<br>#48<br>#10<br>#16<br>#30<br>#40<br>#50<br>#100<br>#200 | 100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>97.8<br>97.2<br>94.6<br>92.1<br>91.6<br>89.1<br>84.7<br>81.0<br>75.4<br>59.4<br>52.5 |         |        |

| Brown, LOAM,  | Soil Description<br>pH = 7.5   | 1   |
|---|--|---|
| PL= 12  | Atterberg Limits   | PI= 14  |
| D <sub>85</sub> = 0.621<br>D <sub>30</sub> = 0.0151<br>C <sub>u</sub> = | Coefficients D <sub>60</sub> = 0.155 D <sub>15</sub> = 0.0020 C <sub>c</sub> = | D <sub>50</sub> = 0.0605<br>D <sub>10</sub> = |
| USCS=   | Classification<br>AASH   | TO= A-6(4)                                    |
|   | Remarks  |   |
|   |  |   |

Sample No.: S-3

Source of Sample: RB-

**Date:** 7-18-03

Location: Stat: 21+50, 2 ft. Rt. "PR-1"

Elev./Depth: 8.5-10 Ft.

PATRIOT ENGINEERING

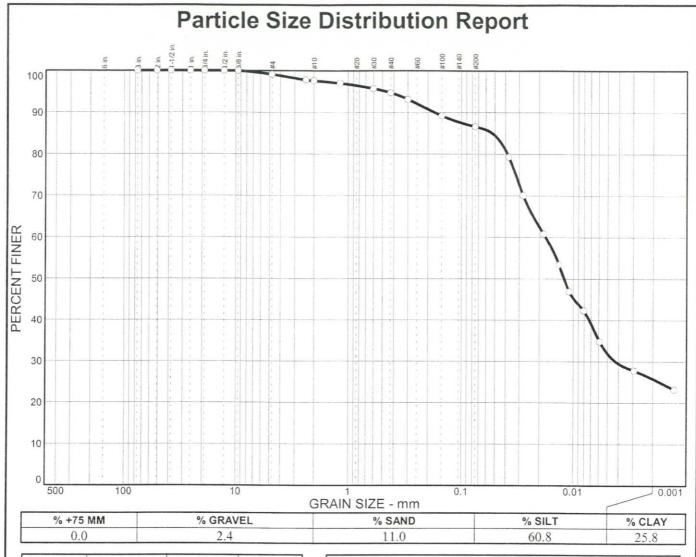
and Environmental, Inc.

Client: Bonar Group

Project: East Pearl Street Road Rehabilitation, Batesville, Indiana

STP 9969(), DES# 0100667

Project No: 1-03-0557



| SIEVE  | PERCENT   | SPEC.*  | PASS?  |
|--|---|---------|--------|
| SIZE   | FINER   | PERCENT | (X=NO) |
| 3 in.<br>2 in.<br>1-1/2 in.<br>1 in.<br>3/4 in.<br>1/2 in.<br>3/8 in.<br>#4<br>#8<br>#10<br>#16<br>#30<br>#40<br>#50<br>#100<br>#200 | 100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>100.0<br>99.1<br>97.8<br>97.6<br>97.0<br>95.7<br>94.7<br>93.1<br>89.2<br>86.6 |         |        |

|  | Soil Description   | 1   |
|--|--|---|
| Gray and brown,  | SILTY CLAY LOA   | M, $pH = 7.4$                                 |
|  |  |   |
| PL= 16   | Atterberg Limits   | PI= 24  |
| D <sub>85</sub> = 0.0528<br>D <sub>30</sub> = 0.0043<br>C <sub>u</sub> = | $\begin{array}{c} \underline{\text{Coefficients}} \\ \text{D}_{60} = 0.0176 \\ \text{D}_{15} = \\ \text{C}_{\text{c}} = \end{array}$ | D <sub>50</sub> = 0.0121<br>D <sub>10</sub> = |
| USCS=  | Classification<br>AASHT  | ΓO= A-6(20)                                   |
|  | Remarks  |   |
|  |  |   |
|  |  |   |

Sample No.: S-1

Source of Sample:

RB-6

**Date:** 7-18-03

Location: Stat: 39+50, 6ft. Lt. "PR-1"

Elev./Depth: 2'-3.5'

## PATRIOT ENGINEERING

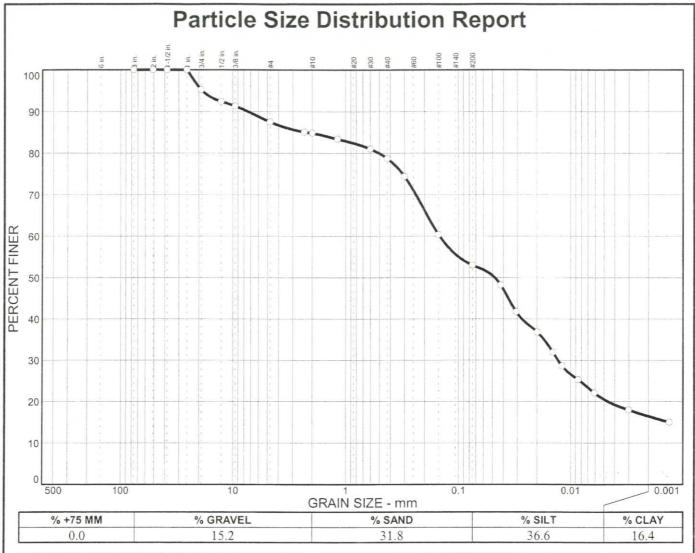
and Environmental, Inc.

Client: Bonar Group

Project: East Pearl Street Road Rehabilitation, Batesville, Indiana

STP 9969(), DES# 0100667

Project No: 1-03-0557



| SIEVE  | PERCENT  | SPEC.*  | PASS?  |
|--|--|---------|--------|
| SIZE   | FINER  | PERCENT | (X=NO) |
| 3 in.<br>2 in.<br>1 -1/2 in.<br>1 in.<br>3/4 in.<br>1/2 in.<br>3/8 in.<br>#44<br>#8<br>#10<br>#16<br>#30<br>#40<br>#50<br>#100<br>#200 | 100.0<br>100.0<br>100.0<br>100.0<br>95.2<br>92.4<br>91.3<br>87.5<br>85.1<br>84.8<br>83.4<br>81.0<br>78.7<br>74.4<br>60.4<br>53.0 |         |        |

|  | Soil Description   |   |
|--|--|---|
| Gray and brown   | , LOAM, $pH = 7.5$   |   |
|  |  |   |
| PL= 13   | Atterberg Limits LL= 28  | PI= 15  |
| D <sub>85</sub> = 2.23<br>D <sub>30</sub> = 0.0130<br>C <sub>u</sub> = | Coefficients D <sub>60</sub> = 0.147 D <sub>15</sub> = 0.0013 C <sub>c</sub> = | D <sub>50</sub> = 0.0478<br>D <sub>10</sub> = |
| USCS=  | Classification<br>AASHT  | O= A-6(4)                                     |
|  | Remarks  |   |
|  |  |   |
|  |  |   |

Sample No.: S-1

Source of Sample: RB-12

Date: 7-18-03

Location: Stat: 25+29, 10 ft. Rt. "B"

Elev./Depth: 1.5-3 Ft.

## PATRIOT ENGINEERING

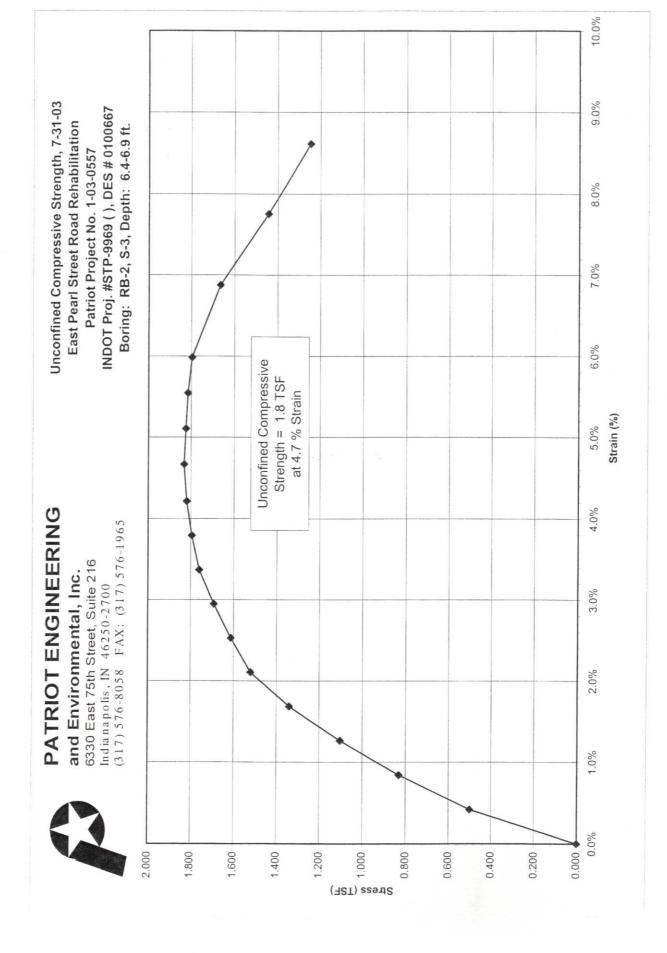
and Environmental, Inc.

Client: Bonar Group

Project: East Pearl Street Road Rehabilitation, Batesville, Indiana

STP 9969(), DES# 0100667

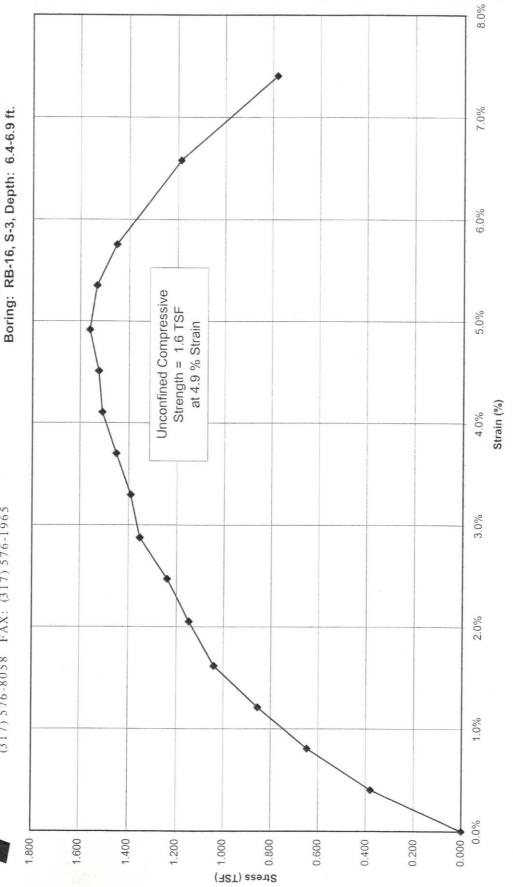
Project No: 1-03-0557





**and Environmental, Inc.** 6330 East 75th Street, Suite 216 Indianapolis, IN 46250-2700 (317) 576-8058 FAX: (317) 576-1965

Unconfined Compressive Strength, 7-31-03
East Pearl Street Road Rehabilitation
Patriot Project No. 1-03-0557
INDOT Proj. #STP-9969 (), DES # 0100667





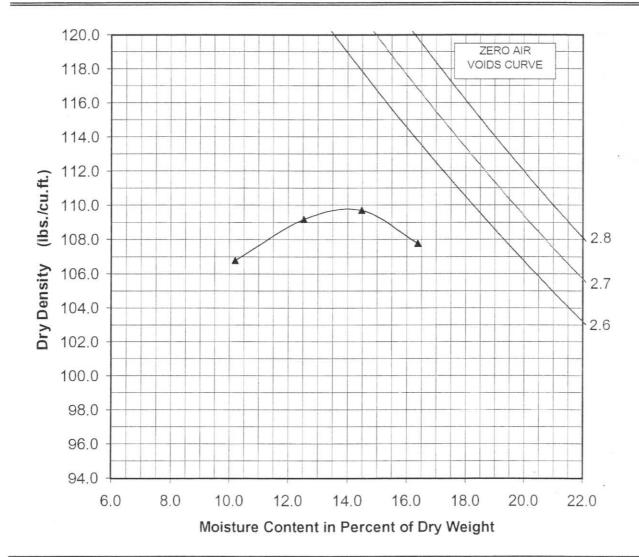
## and Environmental, Inc.

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## Moisture-Density (Proctor)

ASTM D 698, AASHTO T99 (Standard) ASTM D 1557, AASHTO T180 (Modified)

|                 |                                       |                 | Original                     |
|-----------------|---------------------------------------|-----------------|------------------------------|
| Project Name:   | East Pearl Street Road Rehabilitation | Client:         | Bonar Group                  |
| Project Number: | 1-03-0557 (DES# 0100667)              | Client Address: | 6420 Castleway West Drive    |
| Date Received:  | 06/27/2003                            | _               | Indianapolis, IN 46250       |
| Date Tested:    | 07/01/2003                            | Sampled By:     | PM                           |
| Sample Number:  | CBR-1 (RB-3)                          | Tested By:      | RW                           |
| Proctor Type:   | Standard                              | Location_       | Stat: 21+50, 2 ft. Rt "PR-1" |



| Maximum Dry Density: | 110.0pcf              | Optimum Moisture Co         | ntent: 14.0%           |
|----------------------|-----------------------|-----------------------------|------------------------|
| Sample Description:  | Brown, CLAY LOAM,     | pH = 7.6                    |                        |
|                      | LL=40, PL=14, PI=26,  | As Received Moisture = 23%, | Specific Gravity=2.751 |
| Method:              | Manual rammer, proced | dure C                      |                        |



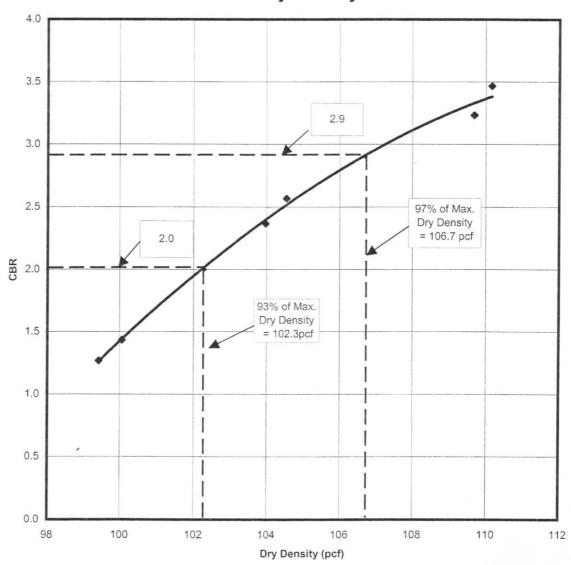
and Environmental, Inc.

## CBR (California Bearing Ratio) of Laboratory-Compacted Soils

| ASTM D | 1883, | AASHTO T1 | 93 |
|--------|-------|-----------|----|
| Origin |       | Amended   |    |

| Project Name:   | East Pearl Street Road Rehabilitation | Client:         | Bonar Group               |
|-----------------|---------------------------------------|-----------------|---------------------------|
| Project Number: | 1-03-0557 (DES #0100667)              | Client Address: | 6420 Castleway West Drive |
| Date Received:  | 06/27/2003                            |                 | Indianapolis, IN 46250    |
| Date Tested:    | 07/12/2003                            | Sampled By:     | PM                        |
| Sample Number:  | CBR-1 (RB-3)                          | Tested By:      | RW                        |
| Location:       | Station: 21+50, 2 ft. Rt."PR-1"       | Sample Source:  | Bulk                      |
|                 |                                       |                 |                           |

# **CBR** vs Dry Density





**and Environmental, Inc.**6330 East 75th Street, Suite 216
Indianapolis, IN 46250-2700
(317) 576-8058 FAX: (317) 576-1965

| Soils               |
|---------------------|
| aboratory-Compacted |
| of L                |
| Ratio)              |
| Bearing             |
| (California         |
| CBR                 |

ASTM D 1883, AASHTO T193

☐ Amended

Original

| Project Name:   | East Pearl Street Road Rehabilitation | Client:         | Bonar Group               |
|-----------------|---------------------------------------|-----------------|---------------------------|
| Project Number: | 1-03-0557 (DES #0100667)              | Client Address: | 6420 Castleway West Drive |
| Sample Number:  | CBR-1 (RB-3)                          |                 | Indianapolis, IN 46250    |
| Location:       | Station: 21+50, 2 ft. Rt."PR-1"       | Sample Source:  | Bulk                      |
| Date Received:  | 06/27/2003 Date Tested: 07/12/2003    | Sampled By:     | PM Tested by: RW          |

# Summary of CBR Test Data

| 25 24.8%<br>25 22.8% |
|----------------------|
| 22.8%                |
| 700 700              |
| %7.17                |
| 24.7%                |
| 23.9%                |



### **AASHTO T 307-99**

# Resilient Modulus of Subgrade Soils and Untreated Base/Subbase Materials (RECOMPACTED / THINWALL TUBE SAMPLES)

|      | LABORATORY: Boudreau Eng                              | gineering, Inc.  | PROJECT NAME:                 | East Pearl Street Rehabilitation |
|------|---|--|-------------------------------|----------------------------------|
|      | Suwanee, Geo  | orgia  | PROJECT NO.:                  | 1-03-0557 (DES 10100667)         |
| D    | ATE RECEIVED: 07-30-200                               | 3  | QUANTITY (REPRESENTED):       |                                  |
| ID   | ENTIFICATION MARKS:                                   | CBR-1 (RB-3)   |                               | CBR-1 (RB-3) at opt. Moisture    |
| 1.   | SAMPLING DATE:  |  |                               | N.R                              |
| 2.   | SAMPLE NUMBER:  |  |                               | CBR-1 op                         |
| 3.   | LAYER TYPE (1 - Subgrade,                             | 2 - Base/Subbase)  |                               | CDK-1 OD                         |
| 4.   | MATERIAL TYPE (Type 1 o                               |  |                               | 4                                |
| 5.   |   |  | SAMPLE, ft (for tube samples) | N/A                              |
| 6.   | TEST INFORMATION                                      |  | or the samples,               | 14/3                             |
|      | PRECONDITIONING - GRA                                 | EATER THAN 5% PERM.  | STRAIN? (Y = YES OR N = NO)   | _                                |
|      | TESTING - GREATER THA                                 |  |                               | <u> </u>                         |
|      | TESTING - NUMBER OF L                                 |  |                               | 15                               |
| 7.   | SPECIMEN INFO.:                                       |  |                               | 10                               |
|      | SPECIMEN DIAM., inch                                  |  |                               |                                  |
|      | TOP   |  |                               | 2.9                              |
|      | MIDDLE  |  |                               | 2.9                              |
|      | BOTTOM  |  |                               | 2.9                              |
|      | AVERAGE   |  |                               | 2.9                              |
|      | MEMBRANE  | THICKNESS (1), inch  |                               | 0.00                             |
|      | MEMBRANE  | THICKNESS (2), inch  |                               | 0.00                             |
|      | NET DIAM., inch                                       |  |                               | 2.9                              |
|      | HEIGHT OF SPECIMEN, C                                 |  |                               | 5.56                             |
|      | HEIGHT OF CAP AND BAS                                 |  |                               | 0.0                              |
|      | INITIAL LENGTH, Lo , inc                              | ch   |                               | 5.6                              |
|      | INITIAL AREA, Ao, in^2                                |  |                               | 6.5                              |
|      | INITIAL VOLUME Ao Lo , i                              |  |                               | 36.0                             |
| 0    | INITIAL WEIGHT, lbs (for to                           | ACTUAL CONTRACTOR OF THE PROPERTY OF THE PROPE |                               | N/A                              |
| 8.   | SOIL SPECIMEN WEIGHT (for a<br>INITIAL WEIGHT OF CONT |  |                               |                                  |
|      | FINAL WEIGHT OF CONTA                                 |  |                               | 1145.40                          |
|      | WEIGHT OF WET SOIL USE                                |  | rams                          | 0.00                             |
| 9.   | SOIL PROPERTIES.:                                     | D, grams   |                               | 1145.40                          |
| ,    | For Remolded Samples:                                 |  |                               |                                  |
|      | IN SITU MOISTURE CONTE                                | ENT (NUCLEAR) %  |                               | 2//4                             |
|      | IN SITU WET DENSITY (NUC                              |  |                               | N/A                              |
|      | or  | - aa, pej  |                               | <u>N/A</u>                       |
|      | OPTIMUM MOISTURE CON                                  | ITENT. %   |                               | 14.0                             |
|      | MAX. DRY DENSITY, pcf                                 |  |                               | 110.0                            |
|      | For Tube Samples:                                     |  |                               | 11000                            |
|      | IN SITU MOISTURE CONTE                                | NT , %   |                               | N/A                              |
|      | MOISTURE CONTENT AFTE                                 | ER RESILIENT MODULU.   | S TESTING, %                  | N/A                              |
|      | WET DENSITY, pcf                                      |  |                               | N/A                              |
| 2.00 | DRY DENSITY, pcf                                      |  |                               | N/A                              |
| 10.  | SPECIMEN PROPERTIES (for                              |  |                               |                                  |
|      | COMPACTION MOISTURE                                   |  |                               | 14.0                             |
|      | MOISTURE CONTENT AFTE                                 |  | S TESTING, %                  | 13.9                             |
|      | COMPACTION DRY DENSI                                  |  |                               | 106.4                            |
|      | TARGET DRY DENSITY, % COMPACTION LEVEL ACH            |  | TARGET MOISTURE CONT          |                                  |
|      | SPECIFIC GRAVITY, Gs                                  |  | DECREE OF CATURATION          | 96.7%                            |
| 11   | OUICK SHEAR TEST                                      | 2.751  | DEGREE OF SATURATION          | 62.7%                            |
|      | STRESS - STRAIN PLOT ATT                              | ACHFD $(V = VFS N = N$   | 01                            |                                  |
|      | TRIAXIAL SHEAR MAXIMUN                                |  |                               | <u>Y</u>                         |
|      | SPECIMEN FAIL DURING                                  | TRIAXIAL SHEAR? (Y =   | YES N = NO)                   | 41<br>N                          |
| 12.  |   | 11-  |                               | <u>N</u><br>08-05-2003           |
|      | GENERAL REMARKS:                                      |  |                               | 00-03-2003                       |
|      |   |  |                               |                                  |
| TES  | TED BY RLB  |  | ATE 09.05.2002                |                                  |
|      | THE REID  |  | DATE 08-05-2003               |                                  |



# Resilient Modulus of Subgrade Soils and Untreated Base/Subbase Materials AASHTO T307-99 REPORT FORM X1.1

LABORATORY: Boudreau Engineering, Inc.

Suwanee, Georgia

PROJECT NAME: PROJECT NO(S):

SOURCE OF MATERIAL: S 8 4

REMOLDING TARGETS:

95% Maximum Dry Density at 14% Moisture Content

LAYER TYPE (1 - subgrade, 2 - base/subbase) 5.

MATERIAL TYPE (Type 1 or Type 2) TEST DATE 6.

RESILIENT MODULUS TESTING

08-05-2003

CBR-1 (RB-3) at opt. Moisture East Pearl Street Rehabilitation

1-03-0557 (DES 10100667)

Resilient Modulus 12,520 12,830 12,888 4 ž psi Resilient 0.00015 0.00015 0.00015 Strain in/in d<sub>3</sub> Recov Def. 0.00085 Average 0.00084 0.00084 #1 Reading #2 Reading LVDT 1 and 2 Havg Ξ Recov. Def. Recov. Def. 0.00083 0.00083 0.00084 LVDT EZ .⊑ 0.00085 0.00085 0.00086 LVDT Ī .⊑ Applied Contact Scontact Actual Stress bsi 0.2 0.2 0.2 Applied Cyclic Scyclic Actual Stress 1.9 1.9 1.9 psi Applied Actual Stress Axia! Smax Мах. psi 2.1 2.1 2.1 Applied Pcontact Actual Contact Load sq Cyclic Load Applied Pcyclic Actual 12.5 12.6 12.4 lbs 2 Max. Axial Applied Actual Pmax Load 13.5 13.7 13.7 lbs Cycle No. 96 97 98 C 1 Maximum Nominal Stress Scyclic Axial 2.0 psi Pressure Confining Chamber 6.0 53 psi DESIGNATION PARAMETER SEQUENCE 1 PRECISION COLUMN # LINO

Report Form X1.1

12,901 12,471 12,722 209

0.00015 0.00015 0.00015 0.0000.0

0.00084 0.00085 0.00084 0.0000.0

0.00083

0.00086

0.2

2.0

2.1

12.7 12.3 12.5

13.8

99

100

0.00083 0.00083 0.0000.0

0.00086

0.2 0.2

1.9 1.9 0.0

0.00086

0.0001

0.0

0.0

0.2

0.1

2.1 2.1

1

13.6 13.4

COLUMN AVERAGE

STANDARD DEV

| Project Name: | East Pearl Street Rehabilitation | et Rehabili | tation |      | Identifica | tion Marks: C | Identification Marks: CBR-1 (RB-3) |     |     | Mate    | Material Source: CBR-1 (RB-3) at opt. Moisture | CBR-1 (RB- | 3) at opt. Mo | isture |
|---------------|----------------------------------|-------------|--------|------|------------|---------------|------------------------------------|-----|-----|---------|--|------------|---------------|--------|
|               | 2.0                              | 8.0         | 96     | 52.0 | 47.4       | 4.7           | 8.0                                | 7.3 | 0.7 | 0.00374 | 0.00371  | 0.00372    | 0.00067       | 10,955 |
|               |                                  |             | 26     | 52.0 | 47.3       | 4.8           | 8.0                                | 7.3 | 0.7 | 0.00374 | 0.00370  | 0.00372    | 0.00067       | 10,930 |
| SEQUENCE 14   |                                  |             | 86     | 52.0 | 47.1       | 4.8           | 8.0                                | 7.3 | 7.0 | 0.00374 | 0.00370  | 0.00372    | 0.00067       | 10,915 |
|               |                                  |             | 66     | 52.0 | 47.2       | 4.8           | 8.0                                | 7.3 | 0.7 | 0.00375 | 0.00371  | 0.00373    | 0.00067       | 10,907 |
|               |                                  |             | 100    | 51.9 | 47.1       | 4.8           | 8.0                                | 7.3 | 0.7 | 0.00374 | 0.00371  | 0.00372    | 0.00067       | 10,884 |
|               | COLUMN AVERAGE                   | /ERAGE      |        | 52.0 | 47.2       | 4.8           | 8.0                                | 7.3 | 0.7 | 0.00374 | 0.00370  | 0.00372    | 0.00067       | 10,918 |
|               | STANDARD DEV                     | DEV.        |        | 0.1  | 0.1        | 0.1           | 0.0                                | 0.0 | 0.0 | 0.00000 | 0.00000  | 0.00000    | 0.00000       | 26     |
|               | 2.0                              | 10.0        | 96     | 64.8 | 58.7       | 6.1           | 10.0                               | 9.1 | 6.0 | 0.00468 | 0.00467  | 0.00467    | 0.00084       | 10,801 |
|               |                                  |             | 26     | 64.8 | 58.7       | 6.1           | 10.0                               | 9.1 | 6.0 | 0.00469 | 0.00465  | 0.00467    | 0.00084       | 10,806 |
| SEQUENCE 15   |                                  |             | 86     | 65.0 | 58.9       | 6.1           | 10.0                               | 9.1 | 6.0 | 0.00469 | 0.00466  | 0.00468    | 0.00084       | 10,830 |
|               |                                  |             | 66     | 64.7 | 58.6       | 6.1           | 10.0                               | 9.1 | 6.0 | 0.00469 | 0.00466  | 0.00468    | 0.00084       | 10,779 |
|               |                                  |             | 100    | 64.7 | 58.6       | 6.1           | 10.0                               | 9.1 | 6.0 | 0.00468 | 0.00467  | 0.00467    | 0.00084       | 10,790 |
|               | COLUMN AVERAGE                   | /ERAGE      |        | 64.8 | 58.7       | 6.1           | 10.0                               | 9.1 | 6.0 | 0.00469 | 0.00466  | 0.00467    | 0.00084       | 10,801 |
|               | STANDARD DEV                     | DEV.        |        | 0.1  | 0.1        | 0.0           | 0.0                                | 0.0 | 0.0 | 0.00001 | 0.00001  | 0.00000    | 0.00000       | 19     |

08-05-2003 RLB TESTED BY

DATE



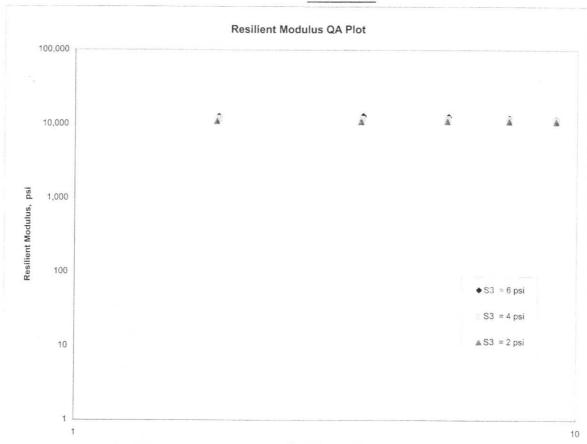
### **AASHTO T307-99**

FIGURE 1 - Logarithmic Plot of Resilient Modulus ( $M_R$ ) vs Cyclic Stress ( $S_C$ )

| 1. | PROJECT NO(S):                            |                 | 1-03-0557 (     | DES 10100667)     |
|----|---|-----------------|-----------------|-------------------|
| 2. | PROJECT NAME:                             |                 | East Pearl Stre | et Rehabilitation |
| 3. | SOURCE OF MATERIAL:                       |                 | CBR-1 (RB-3)    | at opt. Moisture  |
| 4. | REMOLDING TARGETS:                        | 95% Maximum Dry | Density at 14%  | Moisture Content  |
| 5. | LAYER TYPE (1 - subgrade, 2 - base/subbas | se)             |                 | 1                 |
| 6. | MATERIAL TYPE (Type 1 or Type 2)          |                 |                 | 2                 |
| 7. | TEST DATE                                 |                 |                 | 08-05-2003        |

 $M_R = K1 (S_C)^{K2} (S_3)^{K5}$ 

| K1 = | 10,488   |
|------|----------|
| K2 = | -0.02846 |
| K5 = | 0.11790  |
| R2 = | 0.91     |



Cyclic Stress, psi



## **AASHTO T307-99**

## FIGURE 2 - Quick Shear Stress vs Strain

1. PROJECT NO(S):

2. PROJECT NAME:

3. SOURCE OF MATERIAL:

4. REMOLDING TARGETS:

5. LAYER TYPE (1 - subgrade, 2 - base/subbase)

6. MATERIAL TYPE (Type 1 or Type 2)

7. TEST DATE

1-03-0557 (DES 10100667)

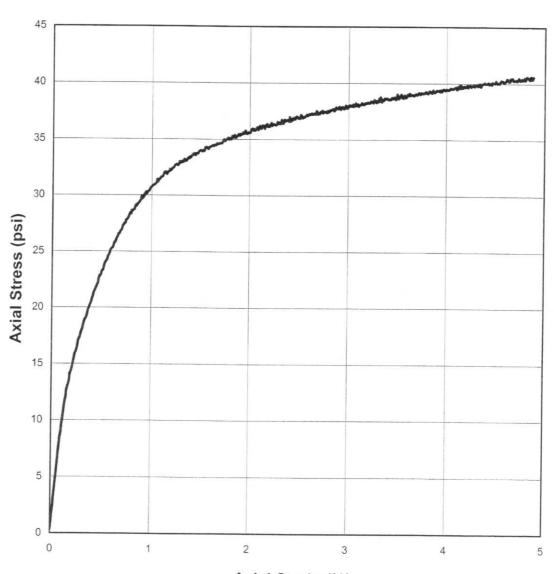
East Pearl Street Rehabilitation

CBR-1 (RB-3) at opt. Moisture

Moisture Content

2

08-05-2003



Axial Strain (%)



### **AASHTO T 307-99**

# Resilient Modulus of Subgrade Soils and Untreated Base/Subbase Materials (RECOMPACTED / THINWALL TUBE SAMPLES)

|      | LABORATORY: Boudres                   | u Engineering,   | Inc.            | PROJECT NAME: East Pearl Street Rehab   | ilitation                |
|------|---------------------------------------|--|-----------------|---|--------------------------|
|      | Suwane                                | e, Georgia   |                 | PROJECT NO.: 1-03-0557 (DES 10100       |                          |
| DA   | TE RECEIVED: 07-3                     | 0-2003   |                 | QUANTITY (REPRESENTED): N.A.            |                          |
| ID   | ENTIFICATION MARKS:                   | CBR  | -1 (RB-3)       | SOURCE OF MATERIAL: CBR-1 (RB-3) at +2% | above opt.               |
| 1.   | SAMPLING DATE:                        |  |                 |   | N.R.                     |
| 2.   | SAMPLE NUMBER:                        |  |                 |   | CBR-1 wet                |
| 3.   | LAYER TYPE (1 - Subg                  | rade, 2 - Base/S   | Subbase)        |   | 1                        |
| 4.   | MATERIAL TYPE (Ty                     |  |                 |   | 2                        |
| 5.   |                                       | ROM TOP OF   | SUBGRADE TO     | SAMPLE, ft (for tube samples)           | N/A                      |
| 6.   | TEST INFORMATION                      |  |                 |   |                          |
|      |                                       |  |                 | STRAIN? (Y = YES OR N = NO)             | N                        |
|      | TESTING - GREATER                     |  |                 |   | N                        |
| -    | TESTING - NUMBER                      | OF LOAD SEQ  | OUENCES COMP    | PLETED (0 - 15)                         | <u>15</u>                |
| 7.   | SPECIMEN INFO.:                       |  |                 |   |                          |
|      | SPECIMEN DIAM., i                     | nch  |                 |   |                          |
|      | TOP                                   | r  |                 |   | 2.9                      |
|      | MIDDL                                 |  |                 |   | 2.9                      |
|      | BOTTO.                                |  |                 |   | 2.9                      |
|      | AVERA(                                |  | 200 (1)         |   | 2.9                      |
|      |                                       | ANE THICKNE  |                 |   | 0.00                     |
|      | NET DIAM., inch                       | ANE THICKNE  | 233 (2), INCN   |   | 0.00                     |
|      | HEIGHT OF SPECIM                      | EN CAPAND  | RASE inch       |   | 2.9                      |
|      | HEIGHT OF CAP AND                     |  | DASE, INCH      |   | 5.55                     |
|      | INITIAL LENGTH, Lo                    | ,  |                 |   | 0.0                      |
|      | INITIAL AREA, Ao, i                   |  |                 |   | <u>5.5</u><br><u>6.5</u> |
|      | INITIAL VOLUME Ao                     |  |                 |   | 35.8                     |
|      | INITIAL WEIGHT, lbs                   |  | les)            |   | N/A                      |
| 8.   | SOIL SPECIMEN WEIGH                   |  |                 |   | MA                       |
|      | INITIAL WEIGHT OF                     |  | * *             | grams                                   | 1167.04                  |
|      | FINAL WEIGHT OF C                     |  |                 |   | 0.00                     |
|      | WEIGHT OF WET SOIL                    |  |                 |   | 1167.04                  |
| 9.   | SOIL PROPERTIES.:                     |  |                 |   | 31.07107                 |
|      | For Remolded Samples:                 |  |                 |   |                          |
|      | IN SITU MOISTURE C                    | ONTENT (NUC  | LEAR), %        |   | N/A                      |
|      | IN SITU WET DENSITY                   | (NUCLEAR),   | pcf             |   | N/A                      |
|      | or                                    |  |                 |   |                          |
|      | OPTIMUM MOISTURI                      | E CONTENT. 2   | 6               |   | 14.0                     |
|      | MAX. DRY DENSITY,                     | pcf  |                 |   | 110.0                    |
|      | For Tube Samples:                     |  |                 |   |                          |
|      | IN SITU MOISTURE C                    |  |                 |   | N/A                      |
|      | MOISTURE CONTENT                      | AFTER RESIL  | IENT MODULUS    | S TESTING, %                            | N/A                      |
|      | WET DENSITY, pef                      |  |                 |   | N/A                      |
| 10   | DRY DENSITY, pcf                      |  |                 |   | N/A                      |
| 10.  | SPECIMEN PROPERTIES                   |  |                 |   |                          |
|      | COMPACTION MOIS                       |  |                 | O TROTTI IC. AL                         | <u>16.0</u>              |
|      | MOISTURE CONTENT                      |  |                 | STESTING, %                             | 15.9                     |
|      | COMPACTION DRY L                      | And the second s | pcf             | TARCET MOJETURE COMPRISE W              | 107.0                    |
|      | TARGET DRY DENSIT<br>COMPACTION LEVEL | -  | <u>95</u>       | TARGET MOISTURE CONTENT, %              | 16.0                     |
|      | SPECIFIC GRAVITY,                     |  | 2.751           | DECREE OF CATURATION IV                 | 97.3%                    |
| 11.  |                                       | US   | 2.751           | DEGREE OF SATURATION, %                 | 72.8%                    |
| 1.1. | STRESS - STRAIN PLO                   | TATTACHED  | (V - VES N - N) | 101                                     |                          |
|      |                                       |  |                 | D/X-SECTION AREA), psi                  | <u>Y</u>                 |
|      | SPECIMEN FAIL DUR                     |  |                 |   | <u>27</u>                |
| 12.  | TEST DATE                             | imaaa  | L SHERRING LL   | 1.00,11-110)                            | N 09 05 2002             |
|      | LOI DITTE                             |  |                 |   | 08-05-2003               |
| 13.  | GENERAL REMARKS:                      |  |                 |   |                          |
| rec  | TED DV                                |  |                 |   |                          |
| ES   | TED BY RLB                            |  |                 | DATE 08-05-2003                         |                          |



# Resilient Modulus of Subgrade Soils and Untreated Base/Subbase Materials AASHTO T307-99 REPORT FORM X1.1

LABORATORY: Boudreau Engineering, Inc.

Suwanee, Georgia

| (S):       | NAME. |
|------------|-------|
| NON<br>NON | Z     |
| ECI        | FOT   |
| PRO        | DAG   |
| 7          | 0     |

East Pearl Street Rehabilitation

CBR-1 (RB-3) at +2% above opt.

1-03-0557 (DES 10100667)

SOURCE OF MATERIAL:

4. REMOLDING TARGETS:

95% Maximum Dry Density at 16% Moisture Content

LAYER TYPE (1 - subgrade, 2 - base/subbase) 5.

MATERIAL TYPE (Type 1 or Type 2) 6. MATERIAL TYPE (Type 1 or Typ 7. TEST DATE 8. RESILIENT MODULUS TESTING

08-05-2003

| COLUMN #    | -             | 2              | 8     | 4          | 5                      | 9        | 7       | 80       | 6        | 10                            | 11          | 12         | 13        | 41        |
|-------------|---------------|----------------|-------|------------|------------------------|----------|---------|----------|----------|-------------------------------|-------------|------------|-----------|-----------|
|             | Chamber       | Nominal        | Cycle | Actual     | Actual                 | Actual   | Actual  | Actual A | Actual A | Recov. Def. Recov. Def.       | Recov. Def. | Average    | Resilient | Resilient |
|             | Confining     | Maximum        | No.   | Applied    | Applied                | Applied  | Applied | Applied  | Applied  | LVDT                          | LVDT        | Recov Def. | Strain    | Modulus   |
| PARAMETER   | Pressure      | Axial          |       | Max. Axial | Max. Axial Cyclic Load | Contact  | Мах.    | Cyclic   | Contact  | Contact #1 Reading #2 Reading | #2 Reading  | LVDT 1     |           |           |
|             |               | Stress         |       | Load       |                        | Load     | Axial   | Stress   | Stress   |                               |             | and 2      |           |           |
|             |               |                |       |            |                        |          | Stress  |          |          |                               |             |            |           |           |
| DESIGNATION | S3            | Scyclic        | 5     | Pmax       | Pcyclic                | Pcontact | Smax    | Scyclic  | Scontact | Ξ                             | HZ          | Havg       | dз        | Mr        |
| LINO        | psi           | isd            | 1     | lbs        | lbs                    | lbs      | isd     | isd      | psi      | .⊑                            | .Ľ          | .⊑         | in/in     | psi       |
| PRECISION   | -,            |                | 1     |            |                        |          |         | .!       | . !      |                               |             |            |           |           |
|             | 0.9           | 2.0            | 96    | 13.5       | 12.3                   | 1.2      | 2.1     | 1.9      | 0.2      | 0.00102                       | 0.00098     | 0.00100    | 0.00018   | 10,505    |
|             |               |                | 26    | 13.6       | 12.3                   | 1.3      | 2.1     | 1.9      | 0.2      | 0.00102                       | 0.00099     | 0.00100    | 0.00018   | 10,543    |
| SEQUENCE 1  |               |                | 98    | 13.5       | 12.2                   | 1.2      | 2.1     | 1.9      | 0.2      | 0.00102                       | 0.00098     | 0.00100    | 0.00018   | 10,469    |
|             |               |                | 66    | 13.4       | 12.3                   | 1.2      | 2.1     | 1.9      | 0.2      | 0.00101                       | 0.00099     | 0.00100    | 0.00018   | 10,517    |
|             |               |                | 100   | 13.6       | 12.3                   | 1.2      | 2.1     | 1.9      | 0.2      | 0.00102                       | 0.00098     | 0.00100    | 0.00018   | 10,565    |
|             | COLUMN        | COLUMN AVERAGE |       | 13.5       | 12.3                   | 1.2      | 2.1     | 1.9      | 0.2      | 0.00102                       | 0.00099     | 0.00100    | 0.00018   | 10,520    |
|             | STANDARD DEV. | RD DEV.        |       | 0.1        | 0.1                    | 0.0      | 0.0     | 0.0      | 0.0      | 0.00000                       | 0.00000     | 0 00000    | 0 00000   | 37        |

37

0.0000.0

0.0000.0

| 23.7         2.3         4.0         3.7         0.3         0.001           23.9         2.3         4.1         3.7         0.4         0.001           23.9         2.3         4.1         3.7         0.4         0.001           23.7         2.3         4.0         3.7         0.4         0.001           23.9         2.2         4.0         3.7         0.4         0.001           0.1         0.0         0.0         0.0         0.001           35.2         3.6         6.0         5.4         0.6         0.003           35.1         3.6         6.0         5.4         0.6         0.003           35.1         3.5         6.0         5.4         0.6         0.003           0.1         0.0         0.0         0.0         0.003           35.1         3.5         6.0         5.4         0.5         0.003           46.1         4.9         7.9         7.1         0.8         0.0044           46.1         4.9         7.9         7.1         0.8         0.0044           46.0         4.9         7.9         7.1         0.8         0.0044   | Project Name: | East Pearl Street Rehabilitation | habilitatio | _  |      | Identifica | Identification Marks: CBR-1 (RB-3) | BR-1 (RB-3) |     |     | Mate    | erial Source | CBR-1 (RR- | Material Source: CBR-1 (RR-3) at +2% above out | too evo |
|--|---------------|----------------------------------|-------------|----|------|------------|------------------------------------|-------------|-----|-----|---------|--------------|------------|--|---------|
| 97 26.3 23.9 2.3 4.1 3.7 0.4     98 26.2 23.9 2.3 4.1 3.7 0.4     99 26.0 23.7 2.3 4.0 3.7 0.4     100 26.1 23.9 2.2 4.0 3.7 0.3     100 26.1 23.9 2.2 4.0 3.7 0.3     100 26.1 23.9 2.2 4.0 3.7 0.3     100 26.1 23.9 2.3 4.0 3.7 0.3     100 38.6 38.2 3.5 3.6 6.0 5.4 0.6     100 38.6 38.7 35.1 3.6 6.0 5.4 0.6     100 38.6 38.7 35.1 3.6 6.0 5.4 0.6     100 38.6 38.7 35.1 3.6 6.0 5.4 0.6     100 38.6 38.7 35.1 3.6 6.0 5.4 0.6     100 38.6 38.7 35.1 3.6 6.0 5.4 0.6     100 38.6 38.7 35.1 3.6 6.0 5.4 0.6     100 38.6 51.0 46.1 4.9 7.9 7.1 0.8     100 50.9 46.0 4.9 7.9 7.9 7.1 0.8     100 50.9 46.0 4.9 7.9 7.9 7.1 0.8     100 50.9 46.0 4.9 7.9 7.9 7.1 0.8     100 50.9 62.6 56.5 61 9.7 88 10     100 90 62.6 56.5 66.0 97 88 10   |               |                                  |             | 9  | 26.0 | 23.7       | 2.3                                | 4.0         | 3.7 | 0.3 | 0.00197 | 0.00192      | 0.00194    | 0.00035  | 10,494  |
| 98   26.2   23.9   2.3   4.1   3.7   0.4     99   26.0   23.7   2.3   4.0   3.7   0.4     100   26.1   23.9   2.2   4.0   3.7   0.4     STANDARD DEV.   0.1   0.1   0.0   0.0   0.0     6.0   6.0   96   38.8   35.2   3.6   6.0   5.4   0.6     STANDARD DEV.   0.1   0.1   0.0   0.0   0.0     6.0   8.0   96   38.6   34.9   3.6   6.0   5.4   0.6     STANDARD DEV.   0.1   0.1   0.0   0.0   0.0     6.0   8.0   96   51.0   46.1   4.9   7.9   7.1   0.8     6.0   8.0   96   51.0   46.1   4.9   7.9   7.1   0.8     8.1   8.2   3.6   6.0   6.0   0.0   0.0     9.1   9.2   5.0   46.0   4.9   7.9   7.1   0.8     9.2   51.0   46.1   4.9   7.9   7.1   0.8     9.3   51.0   46.1   4.9   7.9   7.1   0.8     9.3   51.0   46.1   4.9   7.9   7.1   0.8     9.4   51.0   46.1   4.9   7.9   7.1   0.8     9.5   51.0   46.0   4.9   7.9   7.1   0.8     9.5   51.0   46.0   4.9   7.9   7.1   0.8     9.5   51.0   46.0   4.9   7.9   7.1   0.8     9.5   51.0   46.0   4.9   7.9   7.1   0.8     9.5   51.0   6.0   6.0   0.0   0.0   0.0     9.7   8.8   1.0     9.8   6.2   56.5   6.1   9.7   8.8   1.0     9.9   62.7   56.6   6.0   9.7   8.8   1.0     9.9   62.7   56.6   6.0   9.7   8.8   1.0     9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   62.7   56.6   6.0   9.7   8.8   1.0     9.0   9.0   9.0   62.6   62.6   62.6   63.6   9.7   8.8   1.0     9.0   9.0   9.0   62.6   62.6   63.6   9.7   8.8   1.0     9.0   9.0   9.0   62.6   62.6   63.6   9.7   8.8   1.0     9.0   9.0   9.0   62.6   62.6   63.6   9.7   8.8   1.0     9.0   9.0   9.0   62.6   63.6   9.7   9.7   8.8   1.0     9.0   9.0   9.0   62.6   63.6   9.7   9.7   8.8   1.0     9.0   9.0   9.0   9.0   9.0   9.0   9.0   9.0   9. |               |                                  | 6           | 71 | 26.3 |            | 2.3                                | 4.1         | 3.7 | 0.4 | 0.00196 | 0.00191      | 0.00194    | 0.00035  | 10,605  |
| 100  | SEQUENCE 2    |                                  | 6           | 80 | 26.2 |            | 2.3                                | 4.1         | 3.7 | 0.4 | 0.00197 | 0.00191      | 0.00194    | 0.00035  | 10,555  |
| COLUMN AVERAGE         26.1         23.9         2.2         4.0         3.7         0.3           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0           6.0         6.0         6.0         36         38.8         35.2         3.6         6.0         5.5         0.6           6.0         6.0         38.8         35.2         3.6         6.0         5.4         0.6           98         38.6         38.7         35.1         3.5         6.0         5.4         0.6           99         38.7         35.1         3.5         6.0         5.4         0.6           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0           6.0         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           FOLD MAN AVERAGE         50.8         45.9         4.9         7.9         7.1         0.8           COLUMN AVERAGE         50.9         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0  |               |                                  | 6           | 6  | 26.0 | 23.7       | 2.3                                | 4.0         | 3.7 | 0.4 | 0.00197 | 0.00191      | 0.00194    | 0.00035  | 10,506  |
| COLUMN AVERAGE         26.1         23.8         2.3         4.0         3.7         0.4           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0         0.0           6.0         6.0         6.0         38.8         35.2         3.6         6.0         5.5         0.0           8.0         6.0         38.7         35.1         3.6         6.0         5.4         0.6           99         38.7         35.1         3.6         6.0         5.4         0.6           99         38.7         35.1         3.6         6.0         5.4         0.6           STANDARD DEV.         0.1         0.1         0.1         0.0         0.0         0.0         0.0           6.0         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           F.O         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           COLUMN AVERAGE         50.9         46.0         4.9         7.9         7.1         0.8           COLUMN AVERAGE         50.9         46.0         4.9         7.9         7   |               |                                  | 1(          | 00 | 26.1 |            | 2.2                                | 4.0         | 3.7 | 0.3 | 0.00197 | 0.00191      | 0.00194    | 0.00035  | 10,548  |
| STANDARD DEV.         0.1         0.1         0.0         <  |               | COLUMN AVERA                     | GE          |    | 26.1 |            | 2.3                                | 4.0         | 3.7 | 0.4 | 0.00197 | 0.00191      | 0.00194    | 0.00035  | 10,542  |
| 6.0 6.0 6.0 96 38.8 35.2 3.6 6.0 5.5 0.6 96 97 38.7 35.1 3.6 6.0 5.4 0.6 97 38.7 35.1 3.6 6.0 5.4 0.6 98 38.6 38.6 34.9 3.6 6.0 5.4 0.6 98 38.7 35.1 3.5 6.0 5.4 0.5 98 38.7 35.1 3.5 6.0 5.4 0.5 98 51.0 0.1 0.1 0.1 0.0 0.0 0.0 0.0 0.0 0.0  |               | STANDARD DEV                     | 7.          |    | 0.1  | 0.1        | 0.0                                | 0.0         | 0.0 | 0.0 | 0.00000 | 0.00000      | 0.00000    | 0.00000  | 44      |
| Second  |               |                                  |             | 9  | 38.8 | 35.2       | 3.6                                | 6.0         | 5.5 | 9.0 | 0.00313 | 0.00303      | 0.00308    | 0.00056  | 9,814   |
| 6.0         38.6         34.9         3.6         6.0         5.4         0.6           99         38.7         35.1         3.5         6.0         5.4         0.5           COLUMN AVERAGE         38.7         35.1         3.5         6.0         5.4         0.5           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0           6.0         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           98         51.0         46.1         4.9         7.9         7.1         0.8           99         51.0         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0         0.0           6.0         10.0         96         62.6         56.5         6.1         9.7         8.8         0.9           6.0         10.0         96         62.5         56.4         6.1         9.7         8.8         0.9           99         62.7         56.6         60         9.7         8.7         8.8         1.0 <td></td> <td></td> <td>6</td> <td>7</td> <td>38.7</td> <td>35.1</td> <td>3.6</td> <td>6.0</td> <td>5.4</td> <td>9.0</td> <td>0.00312</td> <td>0.00303</td> <td>0.00307</td> <td>0.00055</td> <td>9,804</td>  |               |                                  | 6           | 7  | 38.7 | 35.1       | 3.6                                | 6.0         | 5.4 | 9.0 | 0.00312 | 0.00303      | 0.00307    | 0.00055  | 9,804   |
| 6.0         38.7         35.1         3.5         6.0         5.4         0.5           100         38.6         35.1         3.5         6.0         5.4         0.5           COLUMIN AVERAGE         38.7         35.1         3.6         6.0         5.4         0.5           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0         0.0           6.0         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           98         51.0         46.1         4.9         7.9         7.1         0.8           100         50.9         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.1         0.0         0.0         0.0         0.0           6.0         10.0         96         62.6         56.5         6.1         9.7         8.8         0.9           6.0         10.0         96         62.5         56.4         6.1         9.7         8.8         0.9           99         62.7         56.6         6.0         9.7         8.8         0.9         0   | SEQUENCE 3    |                                  | 6           | ∞  | 38.6 | 34.9       | 3.6                                | 0.9         | 5.4 | 9.0 | 0.00311 | 0.00303      | 0.00307    | 0.00055  | 9,771   |
| COLUMN AVERAGE         38.6         35.1         3.5         6.0         5.4         0.5           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0         0.0           6.0         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           6.0         8.0         50.8         45.9         4.9         7.9         7.1         0.8           98         51.0         46.1         4.9         7.9         7.1         0.8           99         51.0         46.1         4.9         7.9         7.1         0.8           COLUMN AVERAGE         50.9         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.1         0.0         0.0         0.0         0.0           6.0         10.0         96         62.6         56.5         6.1         9.7         8.8         0.9           99         62.9         56.7         66.0         9.7         8.8         0.9         9.9   |               |                                  | 6           | 6  | 38.7 | 35.1       | 3.5                                | 0.9         | 5.4 | 0.5 | 0.00311 | 0.00303      | 0.00307    | 0.00055  | 9,821   |
| COLUMN AVERAGE         38.7         35.1         3.6         6.0         5.4         0.6           STANDARD DEV.         0.1         0.1         0.0         0.0         0.0         0.0         0.0           6.0         8.0         51.0         46.1         4.9         7.9         7.1         0.8           6.0         8.0         51.0         46.1         4.9         7.9         7.1         0.8           99         51.0         46.1         4.9         7.9         7.1         0.8           COLUMN AVERAGE         50.9         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.1         0.0         0.0         0.0         0.0           6.0         10.0         96         62.6         56.5         6.1         97         8.8         0.9           99         62.5         56.4         6.0         97         8.8         0.9           99         62.5         56.4         6.0         97         8.8         0.9           99         62.7         56.6         6.0         97         8.8         0.9  |               |                                  | 10          | 00 | 38.6 | 35.1       | 3.5                                | 0.9         | 5.4 | 0.5 | 0.00312 | 0.00304      | 0.00308    | 0.00056  | 9,788   |
| STANDARD DEV.         0.1         0.1         0.0         <  |               | COLUMN AVERAC                    | 3E          |    | 38.7 | 35.1       | 3.6                                | 0.9         | 5.4 | 9.0 | 0.00312 | 0.00303      | 0.00307    | 0.00055  | 9,800   |
| 6.0         8.0         96         51.0         46.1         4.9         7.9         7.1         0.8           97         50.8         45.9         4.9         7.9         7.1         0.8           98         51.0         46.1         4.9         7.9         7.1         0.8           99         51.0         46.1         4.9         7.9         7.1         0.8           COLUMN AVERAGE         50.9         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.1         0.0         0.0         0.0         0.0           6.0         10.0         96         62.6         56.5         6.1         9.7         8.8         0.9           98         62.9         56.7         6.0         9.7         8.8         1.0           99         62.7         56.6         6.0         9.7         8.8         0.9   |               | STANDARD DEV                     | ,           |    | 0.1  | 0.1        | 0.0                                | 0.0         | 0.0 | 0.0 | 0.00001 | 0.00001      | 0.00000    | 0.00000  | 20      |
| 97 50.8 45.9 4.9 7.9 7.1 0.8 98 51.0 46.1 4.9 7.9 7.1 0.8 99 51.0 46.1 4.9 7.9 7.1 0.8 100 50.9 46.0 4.9 7.9 7.1 0.8  COLUMN AVERAGE 50.9 46.0 4.9 7.9 7.1 0.8  STANDARD DEV. 0.1 0.1 0.0 0.0 0.0 0.0 0.0  6.0 10.0 96 62.6 56.5 6.1 9.7 8.8 0.9 98 62.9 56.7 66.6 6.0 9.7 8.8 1.0   |               |                                  |             | CO | 51.0 | 46.1       | 4.9                                | 7.9         | 7.1 | 8.0 | 0.00453 | 0.00446      | 0.00450    | 0.00081  | 8,795   |
| 98 51.0 46.1 4.9 7.9 7.1 0.8 99 51.0 46.1 4.9 7.9 7.1 0.8 100 50.9 46.0 4.9 7.9 7.1 0.8  COLUMN AVERAGE 50.9 46.0 4.9 7.9 7.1 0.8  STANDARD DEV. 0.1 0.1 0.1 0.0 0.0 0.0 0.0 0.0  6.0 10.0 96 62.6 56.5 6.1 9.7 8.8 0.9 99 62.7 56.6 6.0 9.7 8.8 0.9   |               |                                  | .6          | 7  | 8.03 |            | 6.4                                | 7.9         | 7.1 | 0.8 | 0.00454 | 0.00445      | 0.00450    | 0.00081  | 8,767   |
| 100 50.9   46.0   4.9   7.9   7.1   0.8   100  | SEQUENCE 4    |                                  | õ           |    | 51.0 | 46.1       | 4.9                                | 7.9         | 7.1 | 0.8 | 0.00455 | 0.00445      | 0.00450    | 0.00081  | 8,792   |
| COLUMN AVERAGE 50.9 46.0 4.9 7.9 7.1 0.8  STANDARD DEV. 0.1 0.1 0.0 0.0 0.0 0.0  6.0 10.0 96 62.6 56.4 6.1 9.7 8.7 0.9  98 62.9 56.7 66.2 9.7 8.8 0.9  |               |                                  | ő           |    | 51.0 | 46.1       | 6.4                                | 7.9         | 7.1 | 8.0 | 0.00454 | 0.00446      | 0.00450    | 0.00081  | 8,803   |
| COLUMN AVERAGE         50.9         46.0         4.9         7.9         7.1         0.8           STANDARD DEV.         0.1         0.1         0.1         0.0         0.0         0.0         0.0           6.0         10.0         96         62.6         56.5         6.1         9.7         8.8         0.9           98         62.9         56.7         6.2         9.7         8.8         1.0           99         62.7         56.6         6.0         9.7         8.8         0.9   |               |                                  | 10          |    | 50.9 | 46.0       | 4.9                                | 7.9         | 7.1 | 0.8 | 0.00452 | 0.00445      | 0.00449    | 0.00081  | 8,793   |
| 6.0 10.0 96 62.6 56.5 6.1 9.7 8.8 0.9 9.0 98 62.9 56.7 66.0 9.7 8.8 1.0 99 62.7 56.6 6.0 9.7 8.8 0.9   |               | COLUMN AVERAC                    | 3E          |    | 6.03 | 46.0       | 4.9                                | 7.9         | 7.1 | 8.0 | 0.00454 | 0.00446      | 0.00450    | 0.00081  | 8,790   |
| 6.0 10.0 96 62.6 56.5 6.1 9.7 8.8 0.9<br>97 62.5 56.4 6.1 9.7 8.7 0.9<br>98 62.9 56.7 6.2 9.7 8.8 1.0  |               | STANDARD DEV                     |             |    | 0.1  | 0.1        | 0.0                                | 0.0         | 0.0 | 0.0 | 0.00001 | 0.00001      | 0.0000.0   | 0.00000  | 14      |
| 97     62.5     56.4     6.1     9.7     8.7     0.9       98     62.9     56.7     6.2     9.7     8.8     1.0       99     62.7     56.6     6.0     9.7     8.8     0.9   |               |                                  |             |    | 62.6 | 56.5       | 6.1                                | 9.7         | 8.8 | 6.0 | 0.00612 | 0.00603      | 0.00608    | 0.00110  | 7,986   |
| 98 62.9 56.7 6.2 9.7 8.8 1.0<br>99 62.7 56.6 6.0 9.7 8.8 0.9   |               |                                  | 6           |    | 62.5 | 56.4       | 6.1                                | 7.6         | 8.7 | 6.0 | 0.00612 | 0.00603      | 0.00608    | 0.00110  | 7,967   |
| 62.7 56.6 6.0 9.7 8.8 0.9  | SEQUENCE 5    |                                  | 36          |    | 62.9 | 26.7       | 6.2                                | 7.6         | 8.8 | 1.0 | 0.00611 | 0.00604      | 0.00607    | 0.00110  | 8,014   |
|  |               |                                  | 36          |    | 62.7 | 9.99       | 0.9                                | 9.7         | 8.8 | 6.0 | 0.00611 | 0.00603      | 0.00607    | 0.00109  | 8,011   |
| 100 62.6 56.6 6.1 9.7 8.8 0.9 0.00611  |               |                                  | 10          |    | 62.6 |            | 6.1                                | 9.7         | 8.8 | 6.0 | 0.00611 | 0.00604      | 0.00607    | 0.00110  | 7,999   |
| COLUMN AVERAGE 62.7 56.6 6.1 9.7 8.8 0.9 0.00611   |               | COLUMN AVERAG                    | 3E          |    | 62.7 | 9.99       | 6.1                                | 9.7         | 8.8 | 6.0 | 0.00611 | 0.00603      | 0.00607    | 0.00110  | 7,995   |
| STANDARD DEV. 0.1 0.1 0.1 0.0 0.0 0.0 0.00001  |               | STANDARD DEV                     |             |    | 0.1  | 0.1        | 0.1                                | 0.0         | 0.0 | 0.0 | 0.00001 | 0.0000.0     | 0.00000    | 0.00000  | 19      |

| Project Name: | East Pearl Street Rehabilitation | reet Rehabili | tation |      | Identific | ation Marks: | Identification Marks: CBR-1 (RB-3) |     |     | Mate    | rial Source: | Material Source: CBR-1 (RB-3) at +2% above opt. | ·3) at +2% ak | oove opt. |
|---------------|----------------------------------|---------------|--------|------|-----------|--------------|------------------------------------|-----|-----|---------|--------------|---|---------------|-----------|
|               | 2.0                              | 8.0           | 96     | 50.9 | 46.1      | 4.8          | 7.9                                | 7.1 | 0.7 | 0.00491 | 0.00483      | 0.00487   | 0.00088       | 8,119     |
|               |                                  |               | 26     | 6.03 | 46.1      | 4.8          | 7.9                                | 7.1 | 0.7 | 0.00492 | 0.00484      | 0.00488   | 0.00088       | 8,112     |
| SEQUENCE 14   |                                  |               | 86     | 6.03 | 46.1      | 4.8          | 7.9                                | 7.1 | 0.7 | 0.00491 | 0.00483      | 0.00487   | 0.00088       | 8,123     |
|               |                                  |               | 66     | 8.03 | 45.9      | 4.9          | 7.9                                | 7.1 | 8.0 | 0.00491 | 0.00484      | 0.00487   | 0.00088       | 8,090     |
|               |                                  |               | 100    | 9.03 | 45.9      | 4.7          | 7.8                                | 7.1 | 0.7 | 0.00491 | 0.00483      | 0.00487   | 0.00088       | 8,092     |
|               | COLUMN AVERAGE                   | AVERAGE       |        | 50.8 | 46.0      | 8.4          | 7.9                                | 7.1 | 7.0 | 0.00491 | 0.00483      | 0.00487   | 0.00088       | 8,107     |
|               | STANDARD DEV.                    | RD DEV.       |        | 0.1  | 0.1       | 0.0          | 0.0                                | 0.0 | 0.0 | 0.00000 | 0.00000      | 0.00000   | 0.00000       | 15        |
|               | 2.0                              | 10.0          | 96     | 62.7 | 56.6      | 6.1          | 9.7                                | 8.8 | 6.0 | 0.00640 | 0.00635      | 0.00638   | 0.00115       | 7,618     |
|               |                                  |               | 26     | 62.6 | 56.5      | 6.1          | 7.6                                | 8.8 | 6.0 | 0.00642 | 0.00635      | 0.00638   | 0.00115       | 7,602     |
| SEQUENCE 15   |                                  |               | 86     | 62.9 | 2.99      | 6.1          | 9.7                                | 8.8 | 6.0 | 0.00641 | 0.00634      | 0.00638   | 0.00115       | 7,636     |
|               |                                  |               | 66     | 63.0 | 6.99      | 0.9          | 9.7                                | 8.8 | 6.0 | 0.00641 | 0.00636      | 0.00639   | 0.00115       | 7,653     |
|               |                                  |               | 100    | 62.9 | 56.9      | 0.9          | 5.6                                | 8.8 | 6.0 | 0.00642 | 0.00635      | 0.00639   | 0.00115       | 7,642     |
|               | COLUMN AVERAGE                   | VERAGE        |        | 62.8 | 56.7      | 6.1          | 9.7                                | 8.8 | 6.0 | 0.00641 | 0.00635      | 0.00638   | 0.00115       | 7,630     |
|               | STANDARD DEV                     | RD DEV.       |        | 0.1  | 0.2       | 0.0          | 0.0                                | 0.0 | 0.0 | 0.00001 | 0.00001      | 0.00000   | 0.00000       | 21        |
|               |                                  |               |        |      |           |              |                                    |     |     |         |              |   |               |           |

TESTED BY RLB DATE 08-05-2003



## **AASHTO T307-99**

## FIGURE 1 - Logarithmic Plot of Resilient Modulus ( $M_R$ ) vs Cyclic Stress ( $S_C$ )

| 1. | PROJECT NO(S):                            | 1-03-0557 (DES 10100667)                        |
|----|---|---|
| 2. | PROJECT NAME:                             | East Pearl Street Rehabilitation                |
| 3. | SOURCE OF MATERIAL:                       | CBR-1 (RB-3) at +2% above opt.                  |
| 4. | REMOLDING TARGETS:                        | 95% Maximum Dry Density at 16% Moisture Content |
| 5. | LAYER TYPE (1 - subgrade, 2 - base/subbas | re) 1   |
| 6. | MATERIAL TYPE (Type 1 or Type 2)          | 2   |
| 7. | TEST DATE                                 | 08-05-2003                                      |

 $M_R = K1 (S_C)^{K2} (S_3)^{K5}$ 

| K1 = | 10,078   |
|------|----------|
| K2 = | -0.15064 |
| K5 = | 0.09388  |
| R2 = | 0.85     |





## **AASHTO T307-99**

## FIGURE 2 - Quick Shear Stress vs Strain

PROJECT NO(S):

 PROJECT NAME:
 East Pearl Street Rehabilitation

 SOURCE OF MATERIAL:

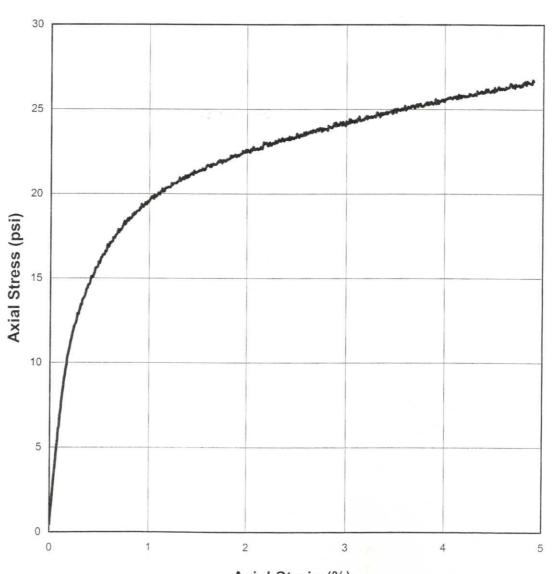
 REMOLDING TARGETS:
 95% Maximum Dry Density at 16% Moisture Content
 Moisture Content

5. LAYER TYPE (1 - subgrade, 2 - base/subbase)

2

6. MATERIAL TYPE (Type 1 or Type 2) 7. TEST DATE

08-05-2003



Axial Strain (%)

# APPENDIX C Alternate Subgrade Treatment For Cut and At-Grade Sections

## **APPENDIX C**

## Alternate Subgrade Treatment for Cut and At-Grade Sections

In this urban setting, some reduction in construction interference with buried utilities may be achieved by a reduction in the amount of over-excavation. Thus, a suggested alternate procedure to the Type A treatment is as follows:

Six (6) inches of subgrade excavated, placement of one layer of geogrid in accordance with INDOT Specification 617, and replacement with coarse aggregate No. 53. If this subgrade treatment is utilized, the pavement design should be based on a CBR value of 2 percent (93 percent compaction).

This recommended procedure may be written on the plans as a Special Provision.